



# REPORT

## KIVALINA CAUSEWAY GEOTECHNICAL REPORT, KIVALINA, ALASKA

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## 1.0 INTRODUCTION

### 1.1 Project Description

Golder Associates Inc. (Golder) has been contracted by the US Army Corps of Engineers, Alaska District (USACE) to perform a subsurface exploration program for the Kivalina Evacuation Road Project in Kivalina, Alaska. The community of Kivalina is located on a barrier island that lies between the Kivalina Lagoon and the Chukchi Sea along the northwest coast of Alaska. Kivalina is located approximately 80 miles northwest of the community of Kotzebue, Alaska, and 75 miles southeast of the community of Point Hope, Alaska. The project location is depicted in the Vicinity Map, Figure 1.

The project consists of an emergency evacuation road crossing the Kivalina Lagoon. The road will incorporate a system of abutments/piers, bridge structures, causeways, and approach roads. At the time of this report, final grades, elevations, spans, and specific design details are not known.

This report provides the results of Golder's review of existing data, geotechnical site exploration, laboratory testing, and discussion of findings. This work was done in accordance with the Statement of Work (SoW) provided by USACE (Statement of Work Revision 10 February 2015 – Contract No. W911KB-13-D-0009), and with the USACE approved Quality Control Plan, Health and Safety Plan, and Geotechnical Work Plan.

### 1.2 Purpose and Scope

Our scope of work consisted of performing a geotechnical site investigation and characterizing the subsurface conditions for the proposed Kivalina Evacuation Road. Golder's findings and geotechnical considerations will support additional engineering design, permitting, and construction cost estimates, all of which will be developed by others. Our scope of services did not include developing geotechnical engineering designs, recommendations, or bid-ready construction documents. Golder's scope of work included:

- Reviewing readily available historical geotechnical explorations within and near the project area.
- Planning and executing a geotechnical drilling program to explore the subsurface soil and thermal conditions along the proposed road alignment up to 50 feet below grade.
- Performing Laboratory testing on samples collected during the geotechnical exploration.
- Providing results of the subsurface exploration and laboratory testing programs in a written Geotechnical Data Report.

Subsurface conditions were characterized by performing a subsurface exploration that included advancing boreholes, collecting soil samples, and laboratory testing. Based on the findings from the field study and laboratory testing, as well as our understanding of the site geology and regional seismic hazards, we are providing a discussion of our analysis.



### 1.3 Project Team

The Golder Project Team consisted of a Project Director, Project Manager, and Team Lead. Mr. Tom Krzewinski, PE, was Project Director and provided senior oversight for the project, while Mr. John Thornley, PE, the Project Manager, was accountable for project planning, monitoring, and closure. Mr. Ryan Campbell was the Team Lead and managed the field exploration program. Drilling services were provided by Discovery Drilling Inc. (Discovery) of Anchorage, Alaska. Logistics and billeting were provided by Remote Site Services Inc. (RSSI) of Anchorage, Alaska.



## 2.0 GEOTECHNICAL SITE INVESTIGATION

### 2.1 Subsurface Drilling and Sampling

The purpose of the drilling program was to explore the subsurface conditions within the project site to determine the physical and engineering characteristics of the soils. The drilling program was conducted between March 14, 2015 and March 21, 2015. Drilling was conducted using a track-mounted Geoprobe 6712DT drill rig, owned and operated by Discovery. A total of six (6) boreholes, identified as K15-01 through K15-06 (Permanent Borehole Numbers AP-39 through AP-44), were advanced at the site, as shown on the Borehole Location Map, Figure 2. The boreholes consisted of two 50-foot boreholes at proposed abutment locations and four 30-foot boreholes along the proposed causeway alignment for a total of 220 linear feet. Each borehole was drilled from the surface of the lagoon ice. The lagoon ice was ground fast at the time the boreholes were drilled.

Drilling was accomplished using hollow-stem auger methods. The augers used during the exploration have an inner diameter of 3.25 inches and an outer diameter of 6.625 inches. Samples were obtained using a 2.0-inch outside diameter (O.D.) split-barrel sampler driven by a 140-pound automatic hammer following the procedures outlined in the American Society of Testing and Materials (ASTM) D1586, "Standard Test Method for Penetration Test and Split Barrel Sampling of Soils." In general, drive samples were collected at 2.5-foot intervals to 17.5 feet, and at 5-foot intervals thereafter to proposed test borehole depths, or at major soil type transitions. In the frozen near surface materials encountered in Boreholes K15-01 (AP-39) and K15-04 (AP-42) where insufficient penetration and material recovery was obtained using the equipment required by the ASTM D1586 test method, a modified penetration test was performed. The modified penetration test included a 3.0-inch O.D. split-barrel sampler and automatic drop hammer set to drop a 340-pound weight a distance of 30 inches.

Samplers were driven into the soil using a 140-pound automatic hammer free-falling a vertical distance of 30 inches. The number of hammer blows or blow counts generally required to drive the sampler in four 6-inch segments were recorded during sampling. The combined blow count for the middle two 6-inch segments is referred to as the uncorrected SPT N-value. Sampling procedures employed in the field were consistent with those described by the American Society for Testing and Materials, ASTM D1586, "Standard Test Method for Penetration Test and Split Barrel Sampling" (2011) with the exception of use of the larger spoon and hammer. Advancement of the SPT sampler was ceased when blow counts to drive the sampler reached 50 blows, in six inches, or more (refusal). Individual blow counts for each sample can be found in the Appendix A, Borehole logs.

Heave was encountered in Borehole K15-01 (AP-39) and K15-04 (AP-42) near the surface at five feet bgs and four feet bgs respectively and was controlled by using the auger wash method. This method uses water poured into the augers to increase the head pressure, to maintain bit circulation while drilling. In all



the boreholes the auger wash method was used to prevent heave. The term “AW” was recorded on the borehole log and sample summary when auger wash methods were used and is indicated on the individual borehole logs and can be found in Appendix A, Borehole Logs.

Each soil sample collected in the field was classified in accordance with ASTM D2488, “Description and Identification of Soils (Visual-Manual Procedure).” Where frozen conditions were encountered, soil samples were also classified in accordance with ASTM D-4083, “Frozen Soil Classification.” Collected soil samples were handled in accordance with ASTM D4220, “Standard Practices of Preserving and Transporting Soil Samples.” The borehole logs are presented in Appendix A. Boundaries between different soil types presented on the logs are approximate because actual transition between layers may be gradual.

### **2.1.1 Site Contamination Screening**

Collected soil samples were placed in plastic bags and warmed to at least 50 degrees Fahrenheit (°F) before beginning the screening process. After about 30 minutes, the samples were screened with a Photoionization Detector (PID) to estimate the presence of volatile organic compound (VOC) levels. The PID used was equipped with a 10.2-electron-volt (eV) lamp. After warming and prior to testing, each sample was shaken or agitated for 15 seconds at the beginning and end of the vapor development period to assist volatilization. After vapor development, the PID sampling probe was inserted to about one-half the headspace depth and the highest meter reading was recorded, which was normally between two and five seconds after probe insertion. Care was taken when inserting the sampling probe into the bag to avoid uptake of any moisture or soil particles. The PID was calibrated at the beginning of every field day with 100-parts per million (ppm) isobutylene calibration gas. As stated in the project’s Final Work Plan<sup>1</sup>, soils with PID readings above 20 ppm, stained, or emitting odors were considered contaminated. Based on the field screenings, no contaminated soils were observed during the exploration.

### **2.1.2 Completion of Boreholes**

Upon completion of drilling, a one-inch diameter, schedule 120 polyvinyl chloride (PVC) pipe was installed in select boreholes to allow for subsurface ground temperature measurements. The annular space between the PVC pipe and the sidewall of the boreholes was backfilled with non-contaminated drill cuttings. In compliance with Golder’s Health and Safety plan, boreholes were not left open overnight without barriers and/or guarding. Horizontal locations were collected using Trimble Geo7x global positioning system (GPS) unit and differentially corrected by post-processing using Trimble GPS Pathfinder software. Post process position accuracy on the observations is between 0 and 50 cm. The borehole locations and elevations are presented in Table 1 below and shown on the Borehole Location

<sup>1</sup> Kivalina Evacuation Road Project, Final Work Plan. Submitted to USACE - Alaska District by Golder Associates Inc. March 6, 2015. Project Number 1419207



Map, Figure 2. Borehole elevations are assumed from bathymetric data provided by USACE on April 30, 2015.

**Table 1: Borehole Locations and Mudline Elevations**

Borehole	Northing (AK83-8F)	Easting (AK83-8F)	Latitude (WGS84)	Longitude (WGS84)	Elevation (Feet) <sup>1</sup>
K15-01 (AP-39)	5021268.196	1842645.871	67.73054419	-164.5427967	-2.34
K15-02 (AP-40)	5021391.276	1842782.222	67.73087171	-164.5417937	-3.38
K15-03 (AP-41)	5021535.562	1842911.126	67.73125763	-164.5408408	-2.14
K15-04 (AP-42)	5021952.875	1843319.69	67.73237149	-164.5378269	-1.85
K15-05 (AP-43)	5022472.143	1843929.111	67.73375086	-164.5333484	-1.4
K15-06 (AP-44)	5023107.386	1844698.75	67.73543656	-164.5276952	-1.77

Notes: Vertical Control is Mean Lower Low Water (MLLW = 0.0' NAVD-88)

<sup>1</sup> Assumed elevations from bathymetric data provided by USACE.

## 2.2 Subsurface Temperature Measurements

Subsurface temperatures were measured in Boreholes K15-01 (AP-39), K15-02 (AP-40), and K15-06 (AP-44) over the period of 30 days following the completion of drilling and recorded as the temperatures stabilized. Subsurface temperatures were measured using a Temperature Acquisition Cable (TAC) with sensor depth spacing of 2.5 feet from the ground surface to 20 feet bgs, and five (5) foot spacing from 20 to 50 feet bgs. Data was recorded on a TAC datalogger that was retrieved by RSSI employee Alex Hawley. Results are presented in Temperature Data Recordings, Appendix C.

## 2.3 Laboratory Testing

A total of 72 representative soil samples were selected for laboratory testing and tested by DOWL of Anchorage, Alaska, a USACE validated geotechnical laboratory. The laboratory testing was performed for the following purposes:

- Substantiating visual field classifications – ASTM D2488
- Classification of Soils (USCS) – ASTM D2487
- Particle-Size Analysis of Soils – ASTM D422
- Moisture Content – ASTM D2216
- Atterberg Limits – ASTM D4318
- Moisture, Ash, and Organic Matter of Peat and Other Organic Soils – ASTM D2974
- Salinity Testing – DOWL In-house procedure
- (Place 100g of material and place in 250ml beaker. Record weight and add equal amount of distilled water and record weight again. Stir samples and let stand



overnight. Determine type of environment samples were recovered from and utilize standard most representative of environment. Stir sample and read temperature and conductivity with conductivity meter.)

Results of laboratory testing are presented in the Laboratory Test Summary, Appendix B. Select laboratory testing results are also presented on the borehole logs in Appendix A.





### 3.0 SITE CONDITIONS

#### 3.1 Regional Setting

Kivalina is within the Arctic Foothills Physiographic Province, which is generally characterized by rolling hills and gentle slopes. The Community of Kivalina; however, is located on the southern end of Kivalina Island, a barrier island that separates Kivalina Lagoon on the east from the Chukchi Sea on the west. The Kivalina River and the Wulik River both flow into Kivalina Lagoon, which in turn discharges into the open sea through the Kivalik Inlet and the Sinauk Entrance.

Kivalina Island is generally less than 20 feet above sea level, is almost flat, and consists of geologically modern beach-sand deposits. Some gravel is present at each end of the island, but historically most granular construction material has been brought in from the Wulik River floodplain. We understand that the only significant source of locally available granular material is from the floodplains and deltas of the two major drainages east of the Kivalina Lagoon.

The Chukchi Sea has a major weather impact on the local climate, but because the Chukchi Sea is frozen for over half the year, Kivalina has a climate that is transitional between Maritime and Continental. The mean annual temperature is about 20°F with an average precipitation rate of less than 10 inches per year. Snowfall is on the order of three feet per year and persistent winter winds can result in significant drifting. Permafrost is present throughout the mainland area east of the Kivalina Lagoon.

Tidal influence in the Kivalina Lagoon is unknown at this time, but the nearest official tide recording station to Kivalina is located at the Red Dog Port, approximately 17 miles to the south. The mean range of tides at the Red Dog Port (9491094) is 0.66 feet from mean sea level according to the National Oceanic and Atmospheric Administration (NOAA)<sup>2</sup>.

#### 3.2 Regional Geology

Bedrock is seldom exposed in the project area except in isolated hills, especially those northwest of the Kivalina floodplain. These hills are topped with rock rubble and outcrops of limestone have been reported. DMA, 2007 see Section 3.3. Kisimigiuktuk Hill, the only hill in or near the project area, is rubble covered.

Although Pleistocene glaciation did not extend to the coast, it has had a major impact on the surficial geology in the Kivalina area. Sea level fluctuation has resulted in the accumulation of sandy beach deposits at various locations both offshore and inland from the presently established coastline. These deposits are similar in composition to present beach deposits, but in many cases they have been partially or totally eroded away or buried by newer fine grained material.

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<sup>2</sup> NOAA Tide and Current Data, <http://tidesandcurrents.noaa.gov/map/>



The drainage patterns of the Wulik and Kivalina Rivers have controlled much of the post-glacial deposition of local sediments. Glacial deposits in the headwaters have been reworked by stream and river action and are the source of gravelly sand and sandy gravel deposits in the modern floodplains. Wind-blown silt and sand is often present as a near-surface veneer that, with surface vegetation, forms the present tundra cover. Along the eastern edge of Kivalina Lagoon, between the two rivers, a vegetation covered and tidally influenced zone extends as much as two miles inland.

Beneath one to two feet of seasonally thawed material, the mainland east of the lagoon is almost universally underlain by permafrost. Horizontally layered ice masses are common and near vertical ice wedges that have developed in soil contraction cracks often result in a surficial feature known as polygonal patterned ground. This segregated ice is generally confined to the fine-grained, organic-rich surface material, but under some conditions ice wedges have penetrated into the underlying granular material.

### 3.3 Existing Geotechnical Data

Golder has conducted geotechnical investigations in Kivalina since the 1990's for infrastructure development projects. Most of our in-house geotechnical data is not located near the proposed evacuation road alignment, although important information about the general subsurface conditions in the area may be applicable. Key elements from our review of historic geotechnical data near the proposed improvements are summarized below.

- **Golder Associates Inc. (Golder) Geotechnical Findings and Conceptual Recommendations, Kivalina Evacuation Road, 2013.** Golder was subcontracted by WHPacific to perform a geotechnical field exploration and provide conceptual-level geotechnical recommendations and considerations for a light-duty, double-lane unpaved roadway. Two roadway alignments, the northern and southern route, were investigated during this program. Based on probe and shallow drill hole data, the southern route was identified as the most viable for the construction of the roadway. The subsurface conditions along the southern alignment generally consisted of approximately 0.5 to 1.5 feet of unfrozen organic mat (PT) overlying approximately two to four feet of frozen silty sand (SM). Five granular material sources for construction of the roadway were also identified.
- **Duane Miller and Associates (DMA), Material Source Desktop Study, 2007.** In 2007 DMA issued a desktop investigation report on potential material targets in and around the Kivalina area. Sandy gravel and sand deposits were identified within the modern floodplains of the Wulik drainage as potential areas for aggregate material assessments. Old beach lines and associated back beach sand dunes were also identified as potential targets for unclassified granular material areas. Rock and rock rubble deposits from bedrock ridges were also identified as potential sources for crushed material.
- **DMA (and others), Permafrost and Wetlands Report, National Guard Armories, Western and Northern Alaska, 2006.** In August 2006, DMA probed for potential active layer depths at the armory in Kivalina. A 30-foot by 30-foot grid was established on the armory site and shallow hand-dug test pits were excavated at two of the grid nodes. Beneath a thin organic mat of grasses and roots, sand with trace fine gravel was



observed to a test pit termination depth of three feet. Frozen ground was not encountered with a five-foot probe in August, although permafrost is expected to be present below the five-foot depth.

- **US Army Corps of Engineers (USACE), Relocation Planning Project 2005.** In December 2005, USACE identified seven potential locations for the relocation of the Village of Kivalina. The purpose of the report was to provide residents and stakeholders with the information necessary to make an informed decision regarding the best solution for the community. Kivalina residents voted several times to choose the new village town site, but could not come to a conclusion as to where the new site would be located.
- **AKDOT & PF, Engineering Geology and Soils Report, Kivalina Airport, 1984.** In August 1984, nine boreholes were drilled in support of a runway expansion in Kivalina. The subsurface profile consisted of a surficial organic mat 0.5 feet thick, underlain by sand to 8 to 14 feet deep. An organic silt layer at least five feet thick was encountered beneath the sand. The active layer was observed at four to six feet below the ground surface and was underlain by permafrost to the depths explored.

### 3.4 Subsurface Conditions

Based on findings from the current geotechnical study, the subsurface conditions along the causeway alignment generally consist of three different sedimentary horizons: 1) lagoonal deposits, 2) nearshore marine deposits, and 3) outwash deposits. The majority of the soils observed in these deposits consisted of silt, organic silt, sandy silt, and silty sand. General soil properties measured in the laboratory for each sedimentary horizon is presented in Table 2. Each sedimentary horizon is discussed in detail in the following section. A geologic cross section along the proposed causeway alignment is shown in Figure 3.

**Table 2: Generalized Soil Properties**

		Sedimentary Horizons		
		Lagoonal Deposits	Nearshore Deposits	Outwash Deposits
USCS Soil Classification (see Note 1)		OL, ML	SP-SM, SM, ML	GW, SW-SM
Organic Content (%)	Average	7	4.5	NA
	Minimum	5.8	4	NA
	Maximum	7.5	5.1	NA
Moisture Content (%)	Average	42	26	15
	Minimum	32	11	6
	Maximum	63	53	31
Salinity (ppt)	Average	8.3	5.7	10.8
	Minimum	2.3	2.7	10.8
	Maximum	15.6	8.6	10.8

Notes: 1. Refer to Appendix A, Figure A-1 for USCS Classification abbreviations.



### 3.4.1 Lagoonal Deposits

Lagoonal deposits generally consist of organic-rich silts, silts with organics, and minor lenses of sand that have been deposited in protected lagoon and bay environments. Locally, the surface layer consists of very soft to firm non-plastic sandy silt ranging from 3 to 17 feet thick and thickening towards the mainland. However, silty sand was encountered at the surface in Boreholes K15-01 (AP-39) and K15-05 (AP-43). The surface layer at Borehole K15-01 (AP-39) may be part of the near shore marine horizon, as a fresh water channel located between Borehole K15-01 (AP-39) and Borehole K15-02 (AP-40) is connected to the Wulik River. Fine grained, organic-rich deposits observed near the bottom of Boreholes K15-01 (AP-39), K15-02 (AP-40), and K15-04 (AP-42) may be older Lagoonal deposits.

### 3.4.2 Nearshore Marine Deposits

Nearshore Marine deposits generally consist of unstructured mixtures of silty sands and sandy silts that have been reworked by grounding sea ice. Locally, Nearshore Marine deposits underlie the surface Lagoonal deposits, and are very loose to dense silty sands interbedded with sandy silt up to 46 feet thick. The Nearshore Marine deposits were the predominant soil types observed in boreholes.

### 3.4.3 Outwash Deposits

Generally, Outwash deposits consist of fluvial and glaciofluvial interbedded gravel and sand with minor silty lenses. These deposits tend to be well-graded sand and gravels with low fines content. Locally, these deposits are dense to very dense well-graded gravel and well-graded sand with silt and gravel. These deposits were observed near the bottom of Boreholes K15-01 (AP-39), K15-02 (AP-40), K15-05 (AP-43) and K15-06 (AP-44), and ranged in thickness from 3.5 to 12.5 feet thick. The Outwash deposits were underlain by older Pleistocene-age Lagoonal deposits.

### 3.4.4 Very Loose Zones

Three very loose zones were encountered during the geotechnical investigation. These very loose zones have SPT blow counts ranging from 0 to 3 blows per foot. Two of the zones are projected between Boreholes K15-01 (AP-39) and K15-02 (AP-40). The first very loose zone is located near the surface approximately 4.5 to 7 feet below mudline and coincides with the fresh water channel. The second very loose zone was encountered at a deeper depth from approximately 22 to 30 feet bgs. The third very loose zone ranges from 7 to 11 feet bgs at Borehole K15-05 (AP-43) and increases in thickness to 5 to 15 feet bgs as it approaches the mainland at Borehole K15-06 (AP-44).

### 3.4.5 Salinity

Salinity was measured in Boreholes K15-03 (AP-41) and K15-06 (AP-44). The salinity measurements in Borehole K15-03 (AP-41), located approximately 500 feet west of the village of Kivalina, ranged from 2.3 to 8.4 parts per thousand (ppt). No permafrost was found in this borehole. The salinity measurements in Borehole K15-06 (AP-44), located approximately 80 feet from the mainland, ranged from 5.2 to 15.6 ppt.



Permafrost was encountered in this borehole from 17 to 31 feet with salinity measurements ranging from 5.2 to 10.8 ppt. In comparison, seawater has a salinity of about 33 ppt and freezes at about 28.7°F.

### 3.4.6 Permafrost

Permafrost was encountered in Boreholes K15-05 (AP-43) and K15-06 (AP-44) within the underlying silty sands at approximate depths of 11 to 21 feet and 17 to 31 feet bgs, respectively. The permafrost is considered poorly-bonded. The measured moisture content in the permafrost soils ranged from 6 to 41 percent and was observed in the field to contain excess non-visible ice. The permafrost encountered in both boreholes may be considered relict permafrost. Relict permafrost is permafrost that has remained from the last sub-aerial exposure of the existing seafloor. During the Pleistocene epoch, 10,000 to 2.6 million years ago, the shallow lagoon may have been exposed to the sub aerial environment during glacial maximums. In addition, the fine grained and organic soils may have insulated the underlying permafrost even after the lagoon was inundated with seawater.

### 3.4.7 Free Water at Depth

Free water at depth was encountered in all of the boreholes while drilling and ranged from 3.0 to 7.0 feet bgs. See Table 3 for individual free water depths per borehole. A fresh water channel was observed flowing between boreholes K15-01 (AP-39) and K15-02 (AP-40) and appears to be an extension of the Wulik River.

**Table 3: Free Water Depths Encountered at Time of Drilling**

Borehole	K15-01 (AP-39)	K15-02 (AP-40)	K15-03 (AP-41)	K15-04 (AP-42)	K15-05 (AP-43)	K15-06 (AP-44)
Depth bgs (ft)	3.0	3.5	7.0	3.5	7.0	6.5



#### 4.0 LIMITATIONS AND USE OF REPORT

This report has been prepared exclusively for the U.S. Army Corps of Engineers (USACE), Alaska District, for the Kivalina Causeway Geotechnical Project in Kivalina, Alaska. The findings, conclusions, and discussion presented in this report are based on visual inspection of the site conditions and limited subsurface exploration data. This report and related work program was prepared in a manner consistent with the level of care and skill ordinarily exercised by other members of the geotechnical engineering profession in the State of Alaska currently practicing under similar conditions and subject to the time limits and financial, physical, and other constraints applicable to the scope of work. No warranty expressed or implied is made.

The construction process is an integral design component with respect to the geotechnical aspects of a project. Geotechnical engineering is not an exact science because of the variability of natural processes. Only a very small portion of the soils that affect the performance of the project have been sampled or observed; thus, variations in subsurface conditions may be present between the shallow explorations authorized under this scope of work and unsampled areas. Variations may also occur with time. Therefore, inspection and testing by a qualified geotechnical engineer should be included during construction to provide corrective recommendations adapted to the conditions revealed during the work. If there are significant changes to the subsurface conditions presented in this report, we should be notified so that we may review our conclusions and provide a written modification or verification of the changes.

The USACE has the responsibility to see that all future parties to the project, including the designer, contractor, subcontractors, etc., are made aware of this report in its entirety. This report contains information that may be useful in the preparation of contract specifications and contractor cost estimates. However, this report is not written as a specification document and may not contain sufficient information for this use without proper modification.



## 5.0 CLOSING

We appreciate the opportunity to provide this report. We are available to provide additional recommendations or comments as necessary. Please contact us at 907-344-6001 if you have questions or comments.

### GOLDER ASSOCIATES INC.

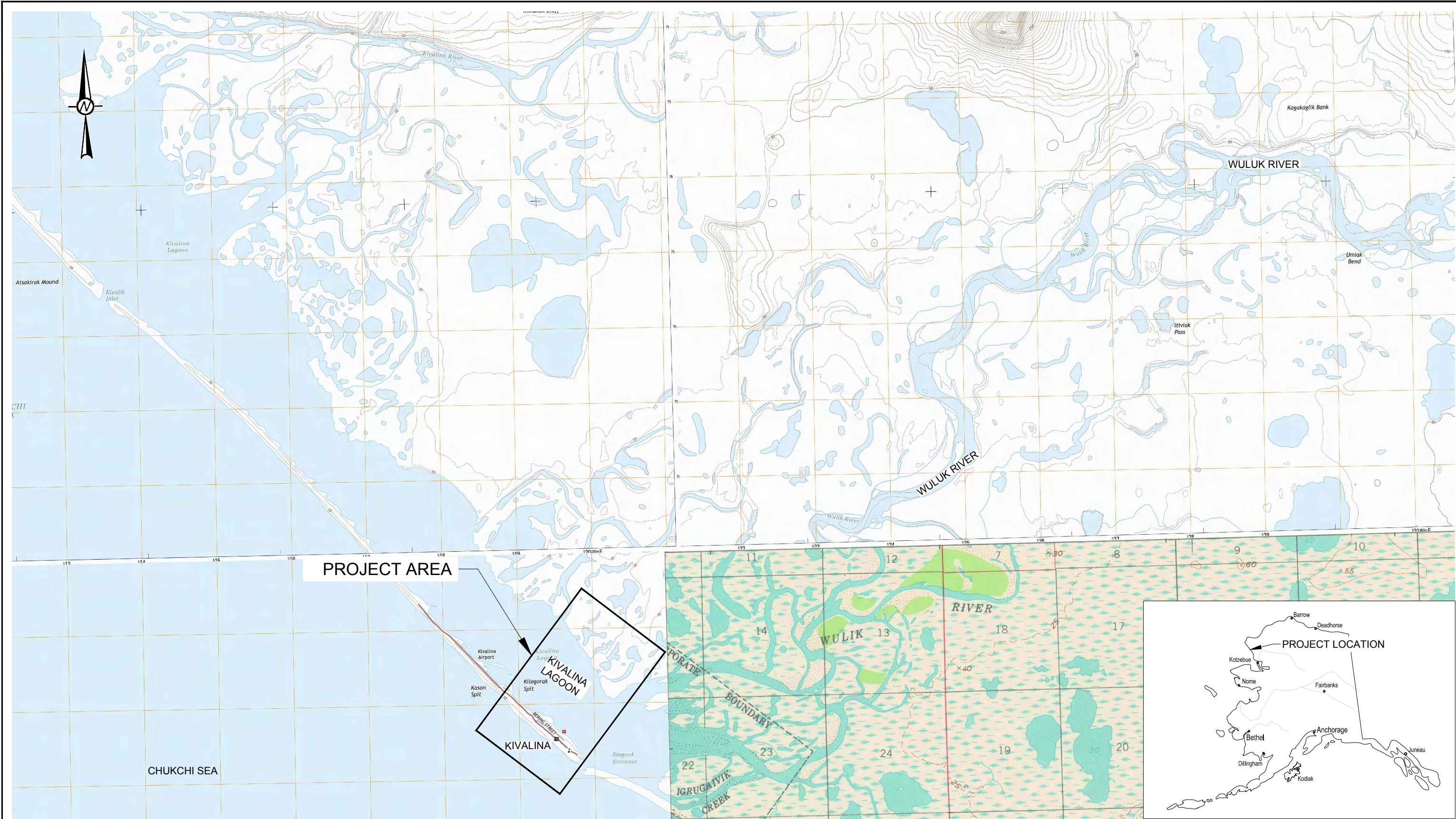
Ryan L. Campbell  
Project Engineering Geologist

John D. Thornley, PE  
Senior Geotechnical Engineer

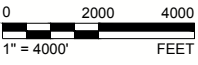
RLC/JDT/SLA/mlp

## FIGURES





**REFERENCE**  
TOPOGRAPHIC MAPS WERE PRODUCED AND DISTRIBUTED BY USGS. 1:25,000 SCALE  
QUADRANGLES USED INCLUDE NOATAK C-5 OW W NE, AK (2014), NOATAK D-5 SW, AK (2014),  
NOATAK D-6 SE, AK (2014). 1:63,360 SCALE QUADRANGLE USED NOATAK (C-5), ALASKA (1982).



**CLIENT**  
U.S. ARMY CORPS OF ENGINEERS - ALASKA DISTRICT

**CONSULTANT**



YYYY-MM-DD	2015-06-01
DESIGNED	-
PREPARED	MSF
REVIEWED	RLC
APPROVED	JDT

**PROJECT**  
KIVALINA CAUSEWAY

**KIVALINA, AK**  
**TITLE**  
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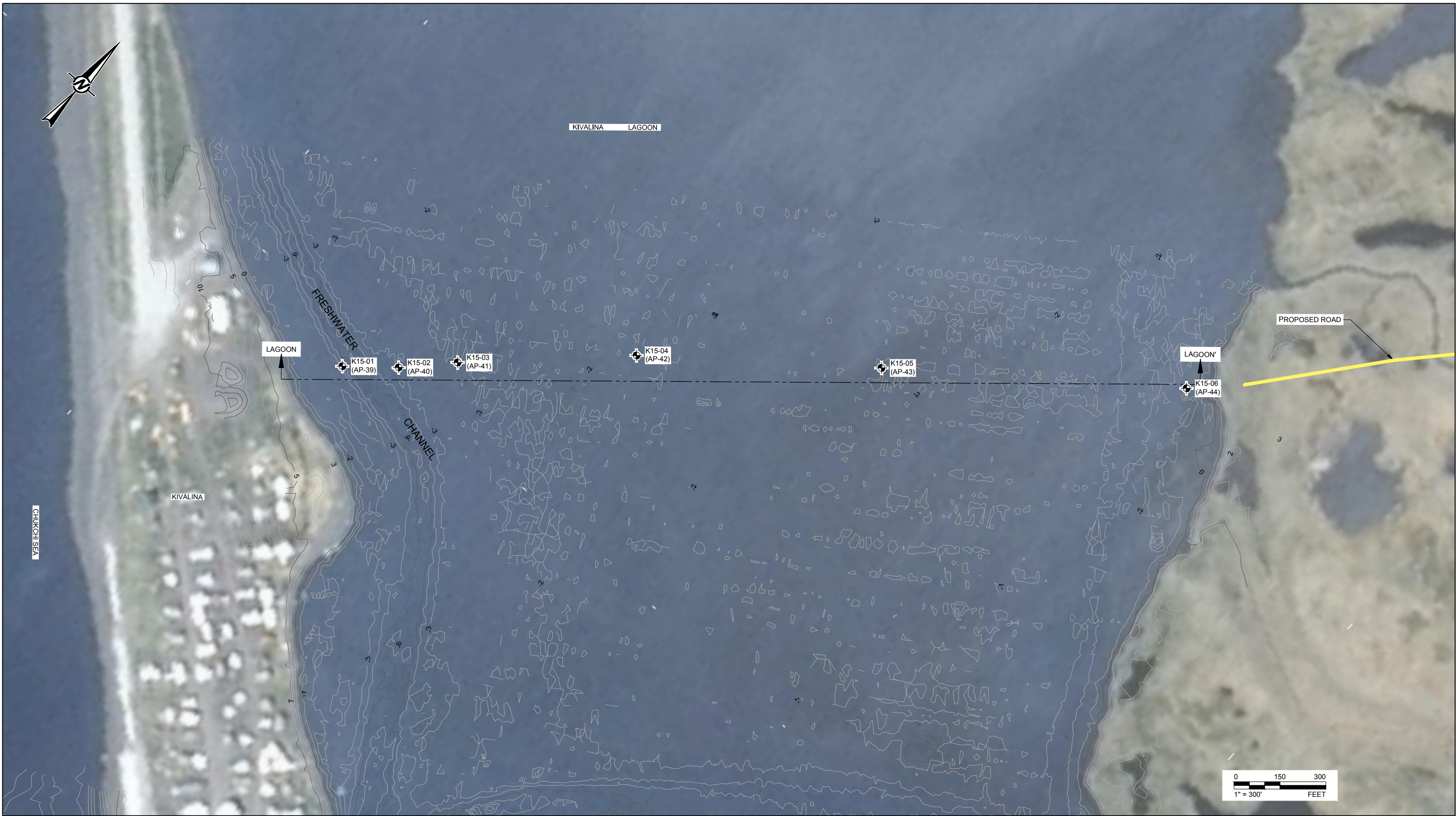
PROJECT NO.	CONTROL	REV.	FIGURE
1419207		A	1

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IF THIS MEASUREMENT DOES NOT MATCH WHAT IS SHOWN, THE SHEET SIZE HAS BEEN MODIFIED FROM ANSI B



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LEGEND

-  K15-01 2015 GOLDER BOREHOLE LOCATION AND NAME
-  (AP-39) PERMANENT BOREHOLE ID

REFERENCE/NOTES

- SPOT IMAGERY FROM 2010 WAS PROVIDED AND DISTRIBUTED BY USGS FROM 1:25,000 SCALE GEOPDF, NOATAK C-5 OW W NE, AK (2014)
- SURFACE/BATHYMETRIC ELEVATION DATA PROVIDED BY USACE ON APRIL 30, 2015
- VERTICAL CONTROL IS MEAN LOWER LOW WATER (MLLW=0.0') BASED ON NAVD88 LOCAL CONTROL VALUES
- HORIZONTAL CONTROL IS AK83-8F
- CONTOUR INTERVAL IS 1' & 5'
- PROPOSED ROAD LOCATIONS PROVIDED BY WHPACIFIC SUMMER 2013

CLIENT  
U.S. ARMY CORPS OF ENGINEERS - ALASKA DISTRICT

CONSULTANT	YYYY-MM-DD	2015-06-01
DESIGNED		-
PREPARED		MSF
REVIEWED		RLC
APPROVED		JDT



PROJECT  
KIVALINA CAUSEWAY

KIVALINA, AK  
TITLE  
BOREHOLE LOCATION MAP

PROJECT NO. 1419207	CONTROL	REV. A	FIGURE 2
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IF THIS MEASUREMENT DOES NOT MATCH WHAT IS SHOWN, THE SHEET SIZE HAS BEEN MODIFIED FROM ANSI B





**APPENDIX A**  
**BOREHOLE LOGS**

# UNIFIED SOIL CLASSIFICATION (adapted from ASTM D2487)

MATERIAL TYPES	CRITERIA FOR ASSIGNING SOIL GROUP NAMES AND GROUP SYMBOLS USING LABORATORY TESTS			GROUP SYMBOL	SOIL GROUP NAMES & LEGEND		
COARSE-GRAINED SOILS >50% RETAINED ON NO. 200 SIEVE	GRAVELS  >50% OF COARSE FRACTION RETAINED ON NO 4. SIEVE	CLEAN GRAVELS <5% FINES	$C_u \geq 4$ AND $1 \leq C_c \leq 3$	GW	WELL-GRADED GRAVEL		If soil contains $\geq 15\%$ sand, add "with sand"
			$C_u < 4$ AND/OR $[C_c < 1$ OR $C_c > 3]$	GP	POORLY GRADED GRAVEL		
		GRAVELS WITH FINES >12% FINES	FINES CLASSIFY AS ML OR MH	GM	SILTY GRAVEL		
			FINES CLASSIFY AS CL OR CH	GC	CLAYEY GRAVEL		
	SANDS  $\geq 50\%$ OF COARSE FRACTION PASSES ON NO 4. SIEVE	CLEAN SANDS <5% FINES	$C_u \geq 6$ AND $1 \leq C_c \leq 3$	SW	WELL-GRADED SAND		If soil contains $\geq 15\%$ gravel, add "with gravel"
			$C_u < 6$ AND/OR $[C_c < 1$ OR $C_c > 3]$	SP	POORLY GRADED SAND		
		SANDS AND FINES >12% FINES	FINES CLASSIFY AS ML OR MH	SM	SILTY SAND		
			FINES CLASSIFY AS CL OR CH	SC	CLAYEY SAND		
FINE-GRAINED SOILS >50% PASSES NO. 200 SIEVE	SILTS AND CLAYS  LIQUID LIMIT <50		CL	LEAN CLAY		If soil contains coarse-grained soil from 15% to 29%, add "with sand" or "with gravel" for whichever type is prominent, or for $\geq 30\%$ , add "sandy" or "gravelly"	
	SILTS AND CLAYS  LIQUID LIMIT $\geq 50$		ML	SILT			
			OL	ORGANIC CLAY OR SILT			
			CH	FAT CLAY			
			MH	ELASTIC SILT			
			OH	ORGANIC CLAY OR SILT			
			HIGHLY ORGANIC SOILS	PT			PEAT

**NOTES:**

$$C_u = \frac{D_{60}}{D_{10}} \quad C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$$

Gravels or sands with 5% to 12% fines require dual symbols (GW-GM, GP-GC, GP-GM, GP-GC, SW-SM, SW-SC, SP-SM, SP-SC) and add "with clay" or "with silt" to group name. If fines classify as CL-ML for GM or SM, use dual symbol GC-GM or SC-SM.  $D_{(X\%)}$  is soil particle diameter where X% is % finer. *Optional Abbreviations:* Lower case "s" after USCS group symbol denotes either "sandy" or "with sand" while "g" denotes either "gravelly" or "with gravel"

## RELATIVE DENSITY / CONSISTENCY ESTIMATE USING STANDARD PENETRATION TEST (SPT) VALUES (adapted from Terzaghi and Peck 1967)

COHESIONLESS SOILS <sup>(a)</sup>		COHESIVE SOILS <sup>(b)</sup>		UNCONFINED COMPRESSIVE STRENGTH (TSF) <sup>(d)</sup>
RELATIVE DENSITY	$(N_1)_{60}$ (blows/ft) <sup>(c)</sup>	CONSISTENCY	$(N_1)_{60}$ (blows/ft) <sup>(c)</sup>	
VERY LOOSE	0 - 4	VERY SOFT	0 - 2	0 - 0.25
LOOSE	4 - 10	SOFT	2 - 4	0.25 - 0.50
COMPACT	10 - 30	FIRM	4 - 8	0.50 - 1.0
DENSE	30 - 50	STIFF	8 - 15	1.0 - 2.0
VERY DENSE	OVER 50	VERY STIFF	15 - 30	2.0 - 4.0
		HARD	OVER 30	OVER 4.0

- (a) Soils consisting of gravel, sand, and silt, either separately or in combination possessing no characteristics of plasticity, and exhibiting drained behavior.
- (b) Soils possessing the characteristics of plasticity, and exhibiting undrained behavior.
- (c) Refer to ASTM D1586 for a definition of N value.  $(N_1)_{60}$  is the N value corrected for hammer energy and overburden pressure, and is detailed in ASTM D6066. N values may be affected by a number of factors including: material size, sampler size, hammer weight and type, depth, drilling method, and borehole disturbance. **N values are only an approximate guide for frozen soil or cohesive soil.**
- (d) Undrained shear strength,  $s_u = 1/2$  unconfined compression strength,  $U_c$ . Note that Torvane (TV) measures  $s_u$  and pocket penetrometer (PP) measures  $U_c$ .

## CRITERIA FOR DESCRIBING MOISTURE CONDITION (adapted from ASTM D2488)

DRY	ABSENCE OF MOISTURE, DUSTY, DRY TO THE TOUCH
MOIST	DAMP BUT NO VISIBLE WATER
WET	VISIBLE FREE WATER, USUALLY SOIL IS BELOW WATER TABLE

## COMPONENT DEFINITIONS BY GRADATION

COMPONENT	SIZE RANGE
BOULDERS	GREATER THAN 12 in.
COBBLES	12 in. to 3 in.
GRAVEL	3 in. to #4 Sieve (4.76 mm)
COARSE GRAVEL	3 in. to 3/4 in.
FINE GRAVEL	3/4 in. to #4 (4.76 mm)
SAND	#4 (4.76 mm) to #200 (0.074 mm)
COARSE SAND	#4 (4.76 mm) to #10 (2.0 mm)
MEDIUM SAND	#10 (2.0 mm) to #40 (0.42 mm)
FINE SAND	#40 (0.42 mm) to #200 (0.074 mm)
SILT & CLAY (FINES)	SMALLER THAN #200 (0.074 mm)

## SAMPLER ABBREVIATIONS

<b>SS</b> SPT Sampler (2 in. OD, 140 lb hammer)	<b>C</b> Core (Diamond Bit)
<b>HD</b> Heavy Duty Split Spoon (3 in. OD, 340 lb hammer)	<b>TW</b> Thin Wall (Shelby Tube)
<b>-BL</b> Brass Liners used in Split Spoon	<b>TP</b> Thin Wall Piston Sampler
<b>CA</b> Continuous Core (Soil in Hollow-Stem Auger)	<b>MS</b> Modified Shelby
<b>GS</b> Grab Sample from Surface / Testpit	<b>MC</b> Geoprobe Macro-Core
<b>AC</b> Auger Charge	<b>RC</b> Air Rotary Cuttings
<b>AW</b> Auger Wash	<b>AG</b> Auger Cuttings

## DESCRIPTIVE TERMINOLOGY FOR PERCENTAGES (ASTM D2488)

DESCRIPTIVE TERMS	RANGE OF PROPORTION
TRACE	0 - 5%
FEW	5 - 10%
LITTLE	10 - 25%
SOME	30 - 45%
MOSTLY	50 - 100%

## LABORATORY TEST AND NOTES ABBREVIATIONS / SYMBOLS

<b>Con</b> Consolidation	<b>PID</b> Photoionization Detector	<b>TXCD</b> Triaxial, Consolidated Drained
<b>Dd</b> Dry Density	<b>PM</b> Modified Proctor (D1557)	<b>TXCU</b> Triaxial, Consolidated Undrained
<b>K</b> Thermal Conductivity	<b>PP</b> Pocket Penetrometer (Field)	<b>TXUU</b> Triaxial, Unconsolidated Undrained
<b>MA</b> Sieve and Hydrometer	<b>PTLD</b> Point Load	<b>W<sub>c</sub></b> Liquid Limit (LL)
<b>NP</b> Non-plastic	<b>SA</b> Sieve Analysis	<b>W<sub>p</sub></b> Plastic Limit (PL)
<b>OLI</b> Organic Loss	<b>SpG</b> Specific Gravity	<b>Ω</b> Soil Resistivity (Res.)
<b>P200</b> Passing #200 Sieve (D1140)	<b>TC</b> Thaw Consolidation/Strain	<b>W</b> Water Level
<b>pH</b> Soil pH	<b>TV</b> Torvane (Field)	<b>W<sub>d</sub></b> Water Level While Drilling




## SOIL CLASSIFICATION / LEGEND

Figure A-1

## FROZEN SOIL CLASSIFICATION (ASTM D4083)

1. DESCRIBE SOIL INDEPENDENT OF FROZEN STATE	CLASSIFY SOIL BY THE UNIFIED SOIL CLASSIFICATION SYSTEM			
2. MODIFY SOIL DESCRIPTION BY DESCRIPTION OF FROZEN SOIL	MAJOR GROUP		SUBGROUP	
	DESCRIPTION	DESIGNATION	DESCRIPTION	DESIGNATION
	Segregated ice not visible by eye	N	Poorly bonded or friable	Nf
			Well bonded	No excess ice Nbn
				Excess ice Nbe
	Segregated ice visible by eye (ice less than 25 mm thick)	V	Individual ice crystals or inclusions	Vx
			Ice coatings on particles	Vc
			Random or irregularly oriented ice formations	Vr
			Stratified or distinctly oriented ice formations	Vs
			Uniformly distributed ice	Vu
3. MODIFY SOIL DESCRIPTION BY DESCRIPTION OF SUBSTANTIAL ICE STRATA	Ice greater than 25 mm thick	ICE	Ice with soil inclusions	ICE+soil type
			Ice without soil inclusions	ICE

## ICE BONDING SYMBOLS

	No ice-bonded soil observed
	Poorly bonded or friable
	Well bonded

## DEFINITIONS

Candled Ice is ice which has rotted or otherwise formed into long columnar crystals, very loosely bonded together.

Clear Ice is transparent and contains only a moderate number of air bubbles.

Cloudy Ice is translucent, but essentially sound and non-pervious

Friable denotes a condition in which material is easily broken up under light to moderate pressure.

Granular Ice is composed of coarse, more or less equidimensional, ice crystals weakly bonded together.

Ice Coatings on particles are discernible layers of ice found on or below the larger soil particles in a frozen soil mass. They are sometimes associated with hoarfrost crystals, which have grown into voids produced by the freezing action.

Ice Crystal is a very small individual ice particle visible in the face of a soil mass. Crystals may be present alone or in a combination with other ice formations.

Ice Inclusions are individual ice masses visible in the face of a soil mass. Inclusions may be present alone or in a combination with other ice formations.

Ice Lenses are lenticular ice formations in soil occurring essentially parallel to each other, generally normal to the direction of heat loss and commonly in repeated layers.

Ice Segregation is the growth of ice as distinct lenses, layers, veins and masses in soils, commonly but not always oriented normal to direction of heat loss.

Massive Ice is a large mass of ice, typically nearly pure and relatively homogeneous.

Poorly-bonded signifies that the soil particles are weakly held together by the ice and that the frozen soil consequently has poor resistance to chipping or breaking.

Porous Ice contains numerous voids, usually interconnected and usually resulting from melting at air bubbles or along crystal interfaces from presence of salt or other materials in the water, or from the freezing of saturated snow. Though porous, the mass retains its structural unity.

Thaw-Stable frozen soils do not, on thawing, show loss of strength below normal, long-time thawed values nor produce detrimental settlement.

Thaw-Unstable frozen soils show on thawing, significant loss of strength below normal, long-time thawed values and/or significant settlement, as a direct result of the melting of the excess ice in the soil.

Well-Bonded signifies that the soil particles are strongly held together by the ice and that the frozen soil possesses relatively high resistance to chipping or breaking.

## FROST DESIGN SOIL CLASSIFICATION <sup>(1)</sup>

FROST GROUP <sup>(2)</sup>	GENERAL SOIL TYPE	% FINER THAN 0.02 mm BY WEIGHT	TYPICAL USCS SOIL CLASS
NFS <sup>(3)</sup> [MOA NFS]	(a) Gravels Crushed stone Crushed rock	0 to 1.5	GW, GP
	(b) Sands	0 to 3	SW, SP
PFS <sup>(4)</sup> [MOA NFS] [MOA F2]	(a) Gravels Crushed stone Crushed rock	1.5 to 3	GW, GP
	(b) Sands	3 to 10	SW, SP
S1 [MOA F1]	Gravelly soils	3 to 6	GW, GP GW-GM, GP-GM, GW-GC, GP-GC
S2 [MOA F2]	Sandy soils	3 to 6	SW, SP SW-SM, SP-SM, SW-SC, SP-SC
F1 [MOA F1]	Gravelly soils	6 to 10	GM, GC, GM-GC, GW-GM, GP-GM, GW-GC, GP-GC
F2 [MOA F2]	(a) Gravelly soils	10 to 20	GW, GP GW-GM, GP-GM, GW-GC, GP-GC
	(b) Sands	6 to 15	SM, SW-SM, SP-SM, SC, SW-SC, SP-SC, SM-SC
F3 [MOA F3]	(a) Gravelly soils	Over 20	GM, GC, GM-GC
	(b) Sands, except very fine silty sands	Over 15	SM, SC, SM-SC
	(c) Clays, PI>12	--	CL, CH
F4 [MOA F4]	(a) Silts	--	ML, MH, ML-CL
	(b) Very fine silty sands	Over 15	SM, SC, SM-SC
	(c) Clays, PI<12	--	CL, ML-CL
	(d) Varved clays or other fine-grained banded sediments	--	CL or CH layered with ML, MH, ML-CL, SM, SC, or SM-SC

- (1) From U.S. Army Corps of Engineers (USACE), EM 1110-3-138, "Pavement Criteria for Seasonal Frost Conditions," April 1984  
(2) USACE frost groups directly correspond to frost groups listed in Municipality of Anchorage (MOA) design criteria manual (DCM), 2007; except as noted.  
(3) Non-frost susceptible  
(4) Possibly frost susceptible, requires lab test for void ratio to determine frost design soil classification. Gravel with void ratio > 0.25 would be NFS; Gravel with void ratio < 0.25 would be S1; Sands with void ratio > 0.30 would be NFS; Sands with void ratio < 0.30 would be S2 or F2



## FROZEN SOIL CLASSIFICATION / LEGEND

Figure  
A-2

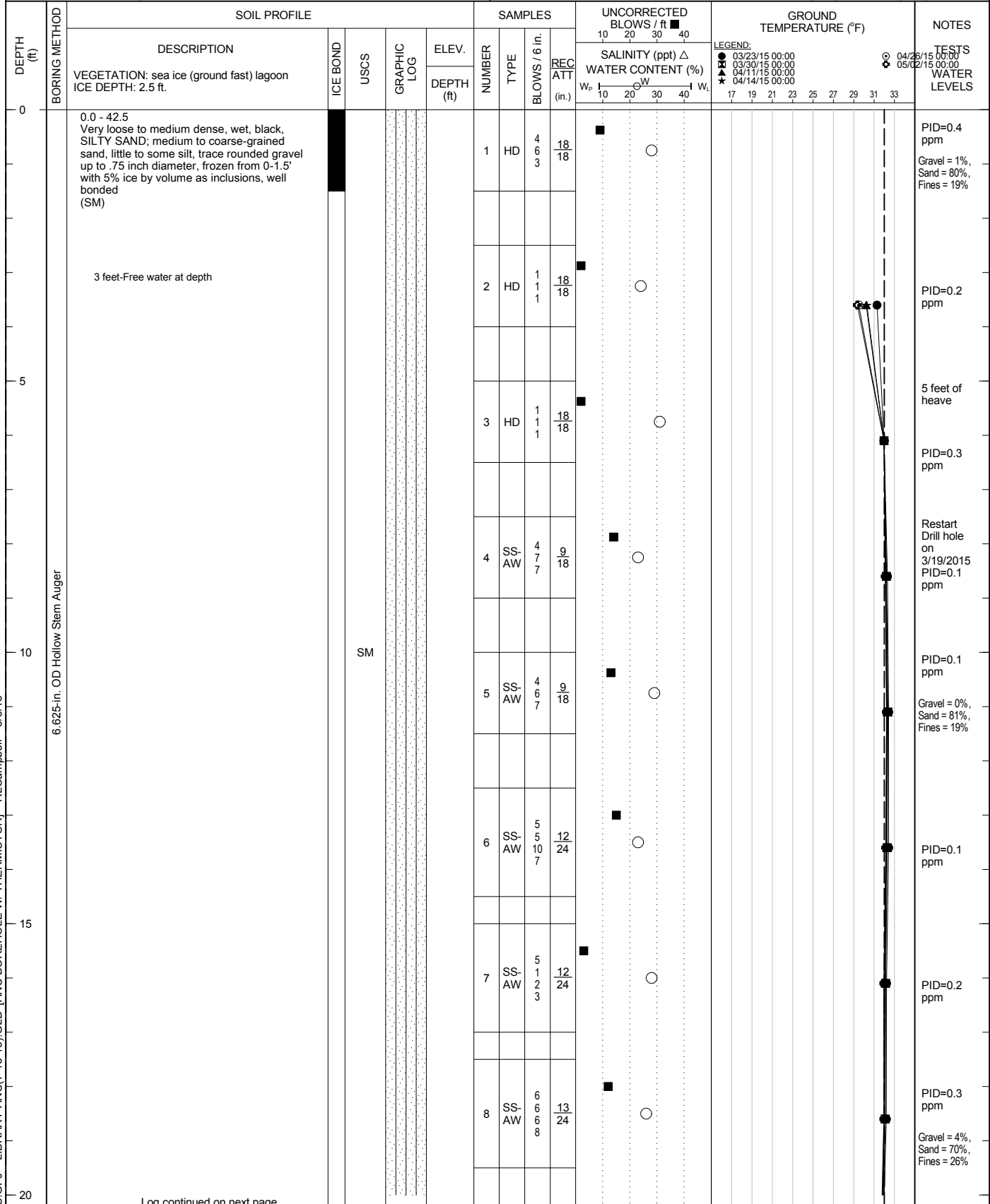
# RECORD OF BOREHOLE K15-01 (AP-39)

SHEET 1 of 3

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-14-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -2.34 ft  
APPROX. COORDS: N: 1,842,646 E: 5,021,268



KIVALINA LOGS.GPJ LIBRARY-ANC(7-15-15).GLB [ANC BOREHOLE W/ THERMISTOR] RLCampbell 8/6/15



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure A-3

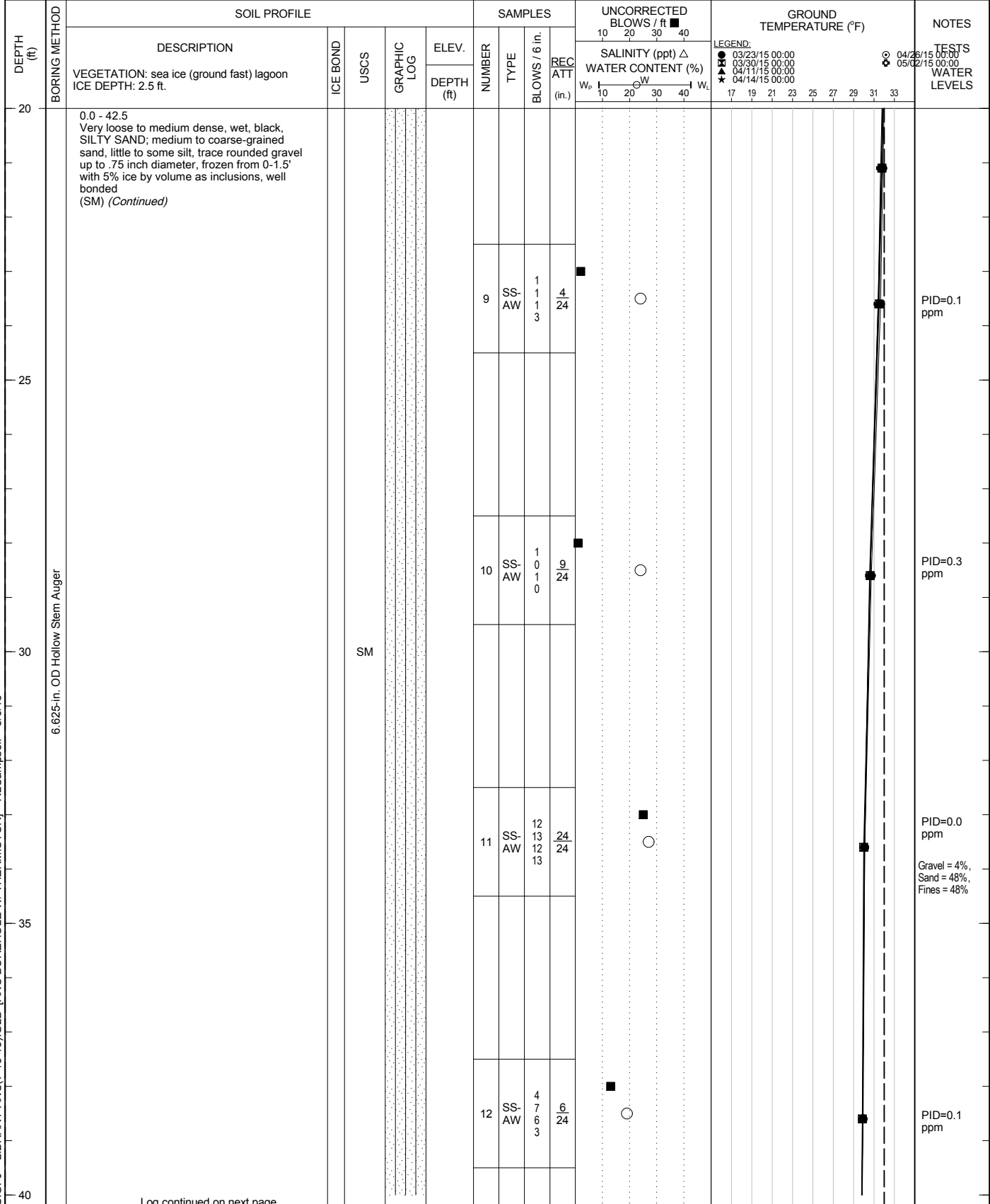
# RECORD OF BOREHOLE K15-01 (AP-39)

SHEET 2 of 3

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-14-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -2.34 ft  
APPROX. COORDS: N: 1,842,646 E: 5,021,268



KIVALINA LOGS.GPJ LIBRARY-ANC(7-15-15).GLB [ANC BOREHOLE W/ THERMISTOR] RLCampbell 8/6/15



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure A-3



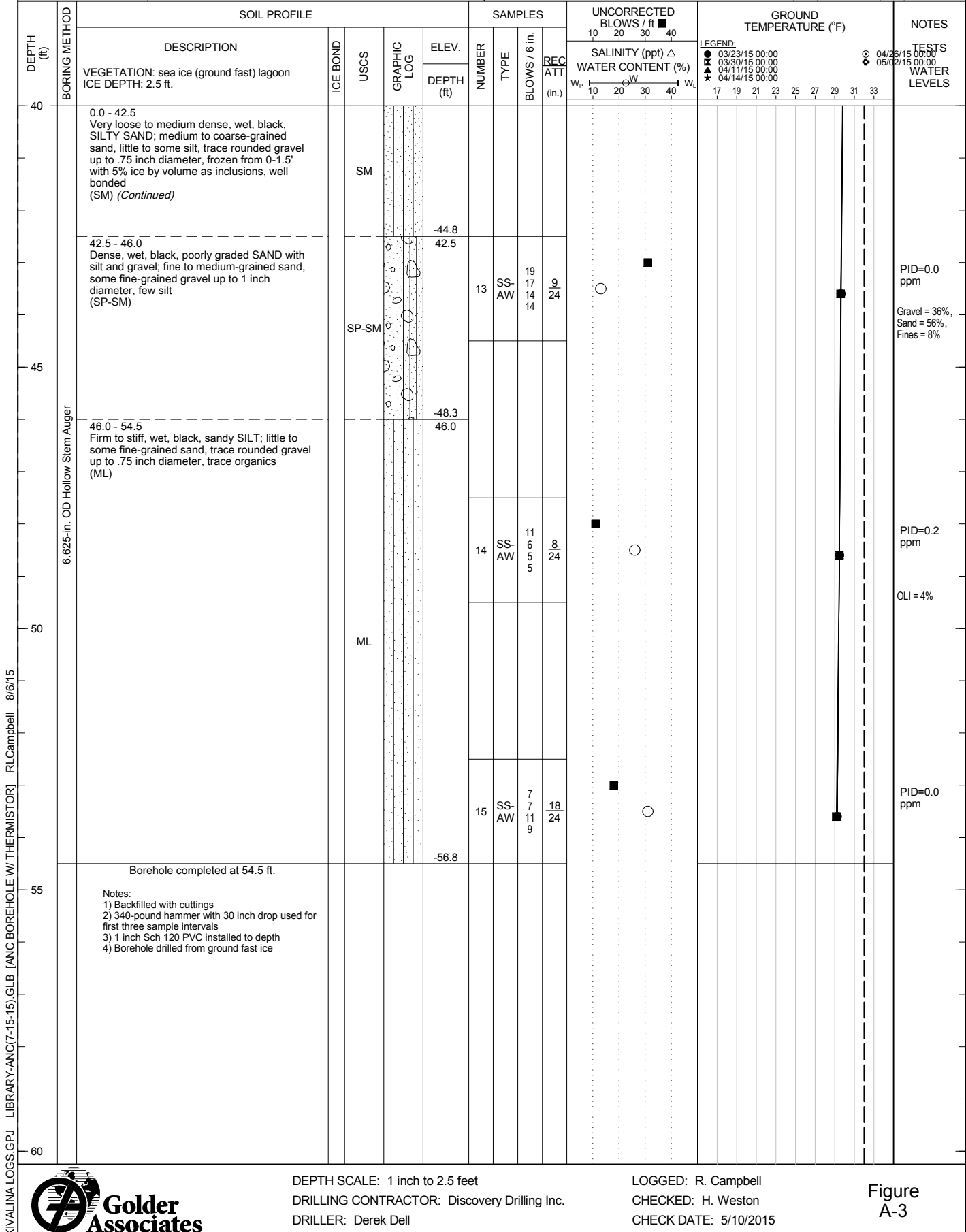
# RECORD OF BOREHOLE K15-01 (AP-39)

SHEET 3 of 3

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-14-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -2.34 ft  
APPROX. COORDS: N: 1,842,646 E: 5,021,268



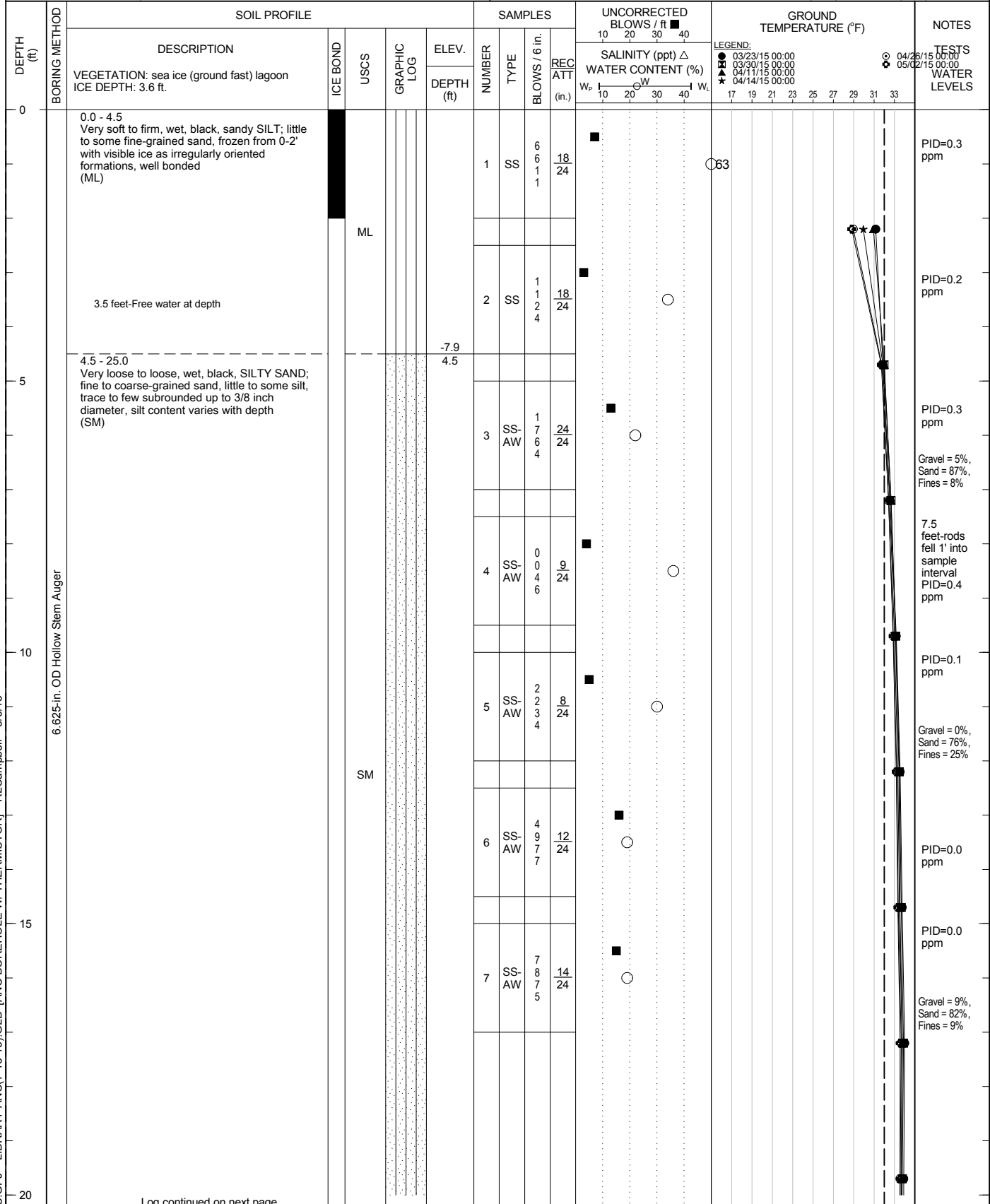
# RECORD OF BOREHOLE K15-02 (AP-40)

SHEET 1 of 3

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-19-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -3.38 ft  
APPROX. COORDS: N: 1,842,782 E: 5,021,391



KIVALINA LOGS.GPJ LIBRARY-ANC(7-15-15).GLB [ANC BOREHOLE W/ THERMISTOR] RLCampbell 8/6/15



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure A-4

## SHEET 2 of 3

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -3.38 ft  
APPROX. COORDS: N: 1.842.782 E: 5.021.391

Log continued on next page

Figure  
A-4



KIVALINA LOGS.GPJ	LIBRARY-ANC(7-15-15).GLB	[ANC BOREHOLE W/ THERMISTOR]	RLCampbell	8/6/15
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## SHEET 3 of 3

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -3.38 ft  
APPROX. COORDS: N: 1,842,782 E: 5,021,391

KIVALINA LOGS.GPJ	LIBRARY-ANC(7-15-15).GLB	[ANC BOREHOLE W/ THERMISTOR]	RLCampbell	8/6/15
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# RECORD OF BOREHOLE K15-03 (AP-41)

SHEET 1 of 2

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-20-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -2.14 ft  
APPROX. COORDS: N: 1,842,911 E: 5,021,536



KIVALINA LOGS.GPJ LIBRARY-ANC(7-15-15).GLB [ANC BOREHOLE W/ THERMISTOR] RLCampbell 8/6/15



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure A-5

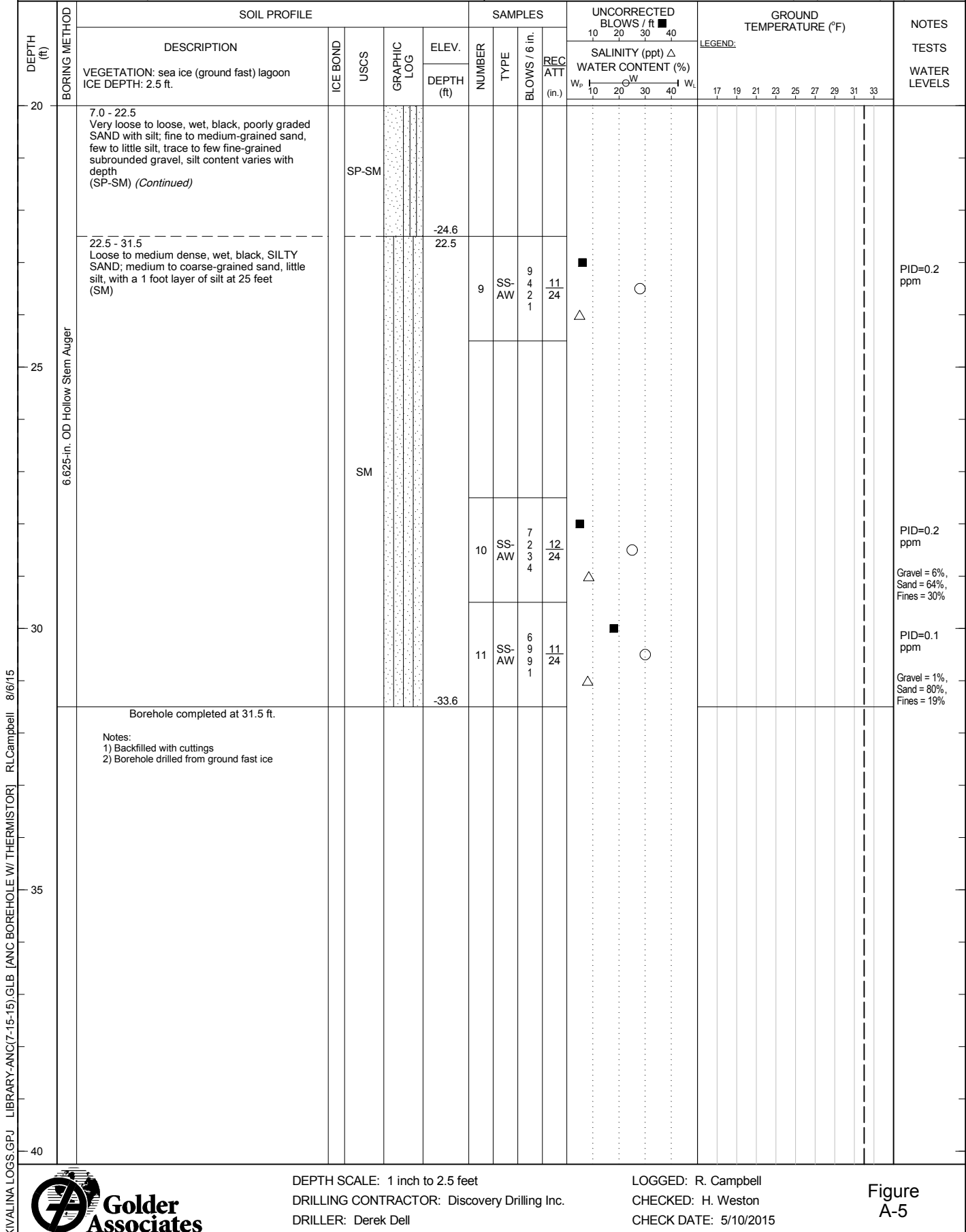
# RECORD OF BOREHOLE K15-03 (AP-41)

SHEET 2 of 2

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-20-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -2.14 ft  
APPROX. COORDS: N: 1,842,911 E: 5,021,536



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure  
A-5

## SHEET 1 of 2

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -1.85 ft  
APPROX. COORDS: N: 1,843,320 E: 5,021,953

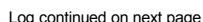


Figure  
A-6



KIVALINA LOGS.GPJ	LIBRARY-ANC(7-15-15).GLB	[ANC BOREHOLE W/ THERMISTOR]	RLCampbell	8/6/15
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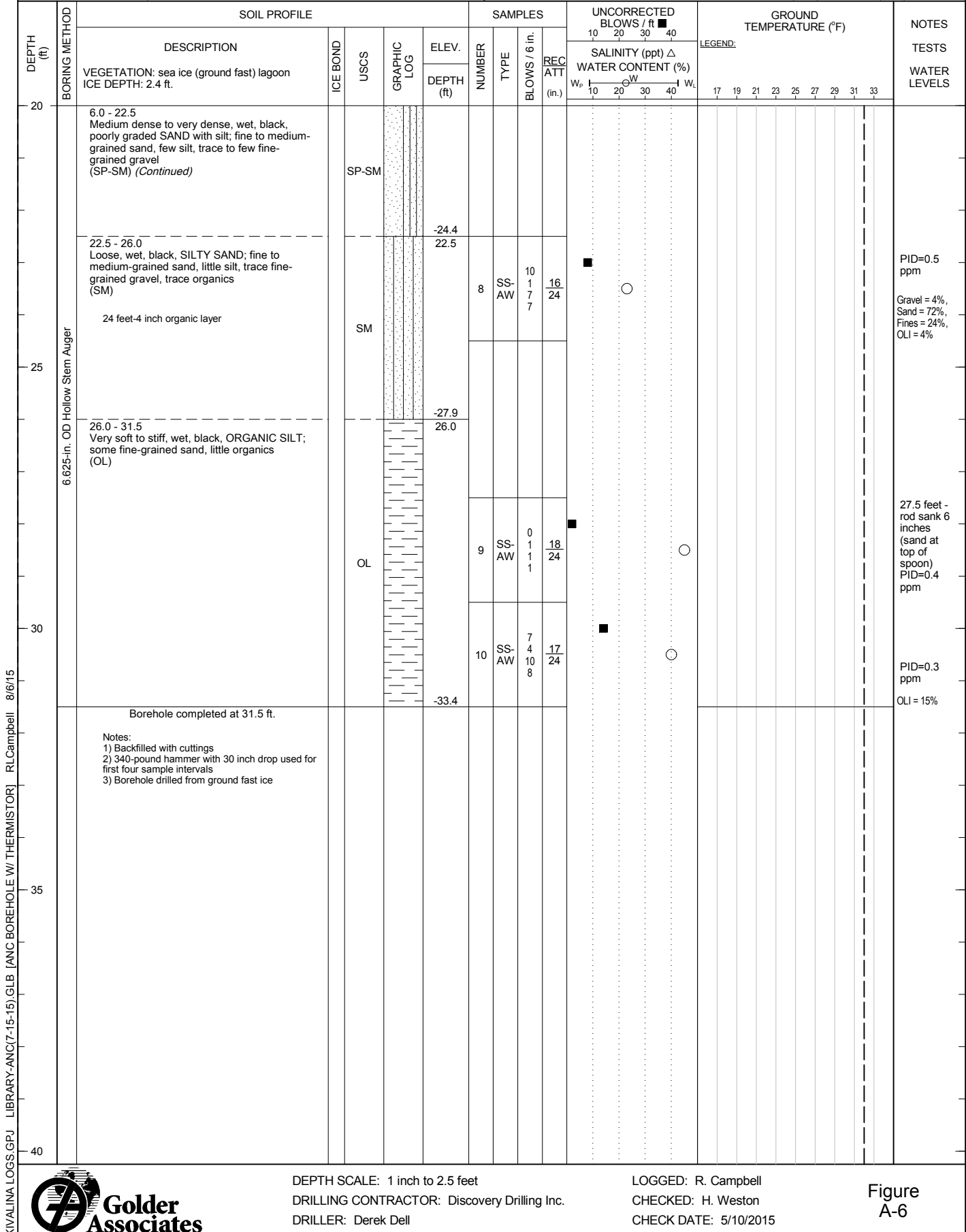
# RECORD OF BOREHOLE K15-04 (AP-42)

SHEET 2 of 2

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-14-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -1.85 ft  
APPROX. COORDS: N: 1,843,320 E: 5,021,953



KIVALINA LOGS.GPJ LIBRARY-ANC(7-15-15).GLB [ANC BOREHOLE W/ THERMISTOR] RLCampbell 8/6/15



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure A-6



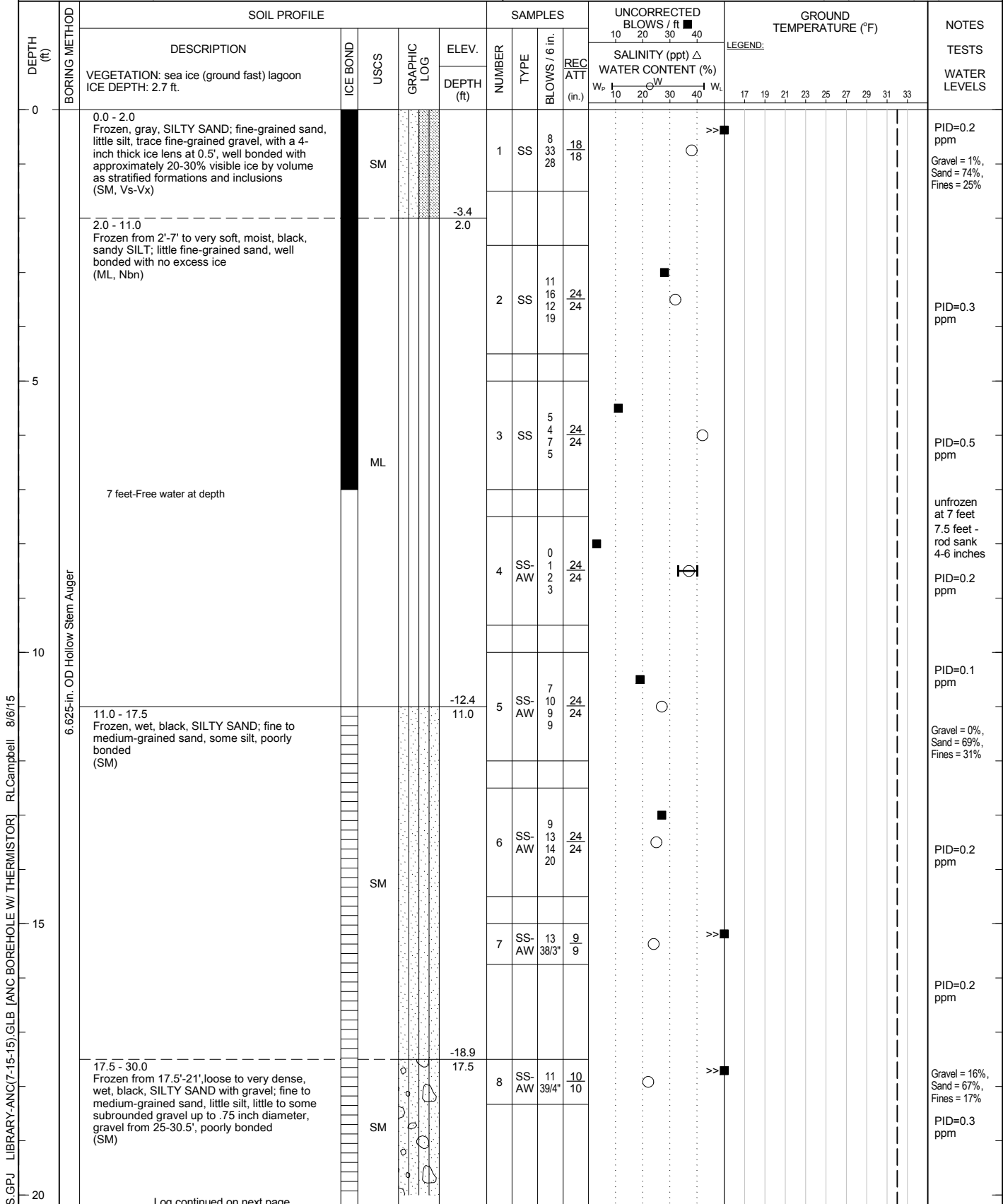
# RECORD OF BOREHOLE K15-05 (AP-43)

SHEET 1 of 2

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-21-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -1.4 ft  
APPROX. COORDS: N: 1,843,929 E: 5,022,472



Log continued on next page



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure  
A-7

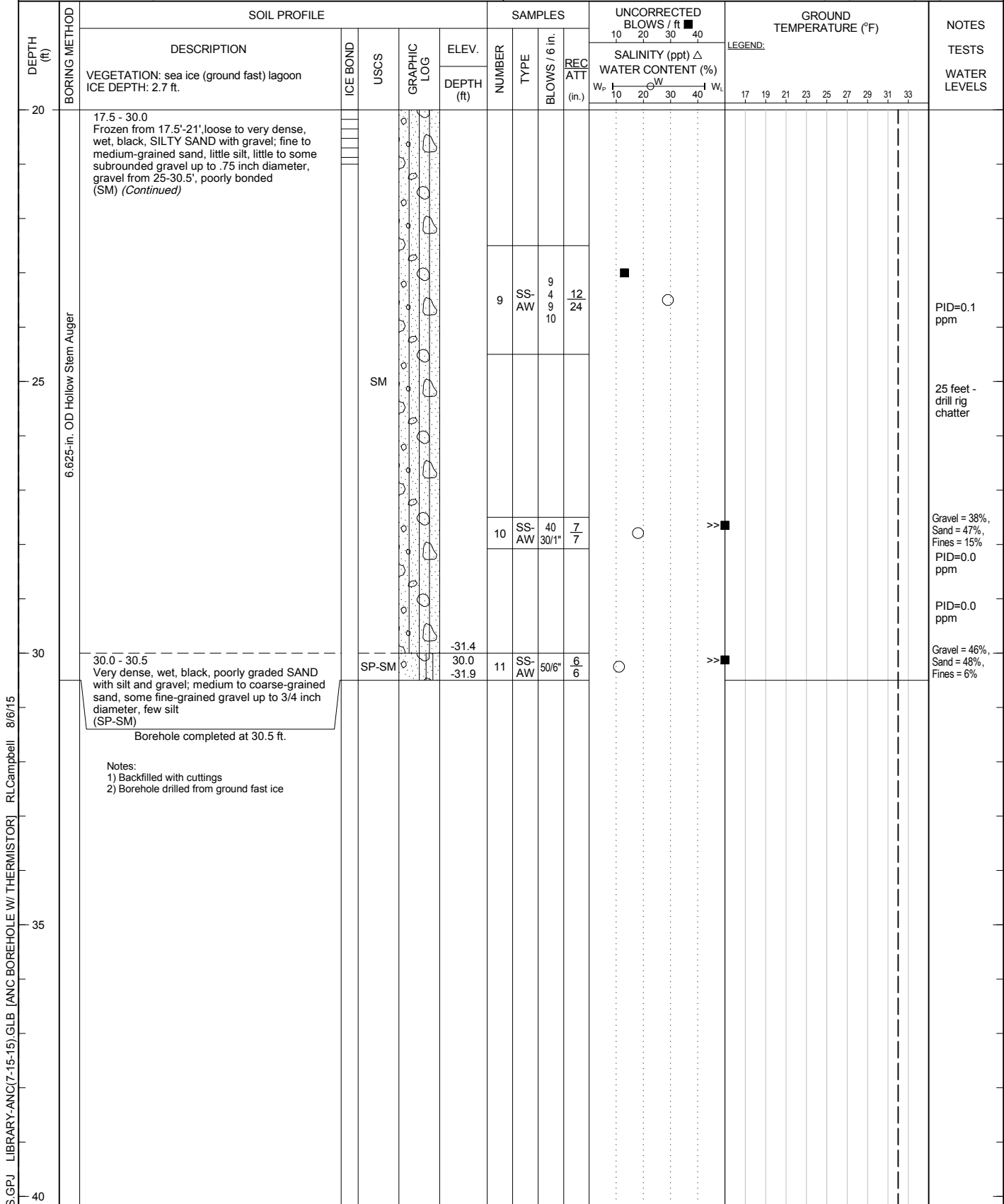
# RECORD OF BOREHOLE K15-05 (AP-43)

SHEET 2 of 2

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-21-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -1.4 ft  
APPROX. COORDS: N: 1,843,929 E: 5,022,472



KIVALINA LOGS.GPJ LIBRARY-ANC(7-15-15).GLB [ANC BOREHOLE W/ THERMISTOR] 8/6/15 RLCampbell



DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure  
A-7

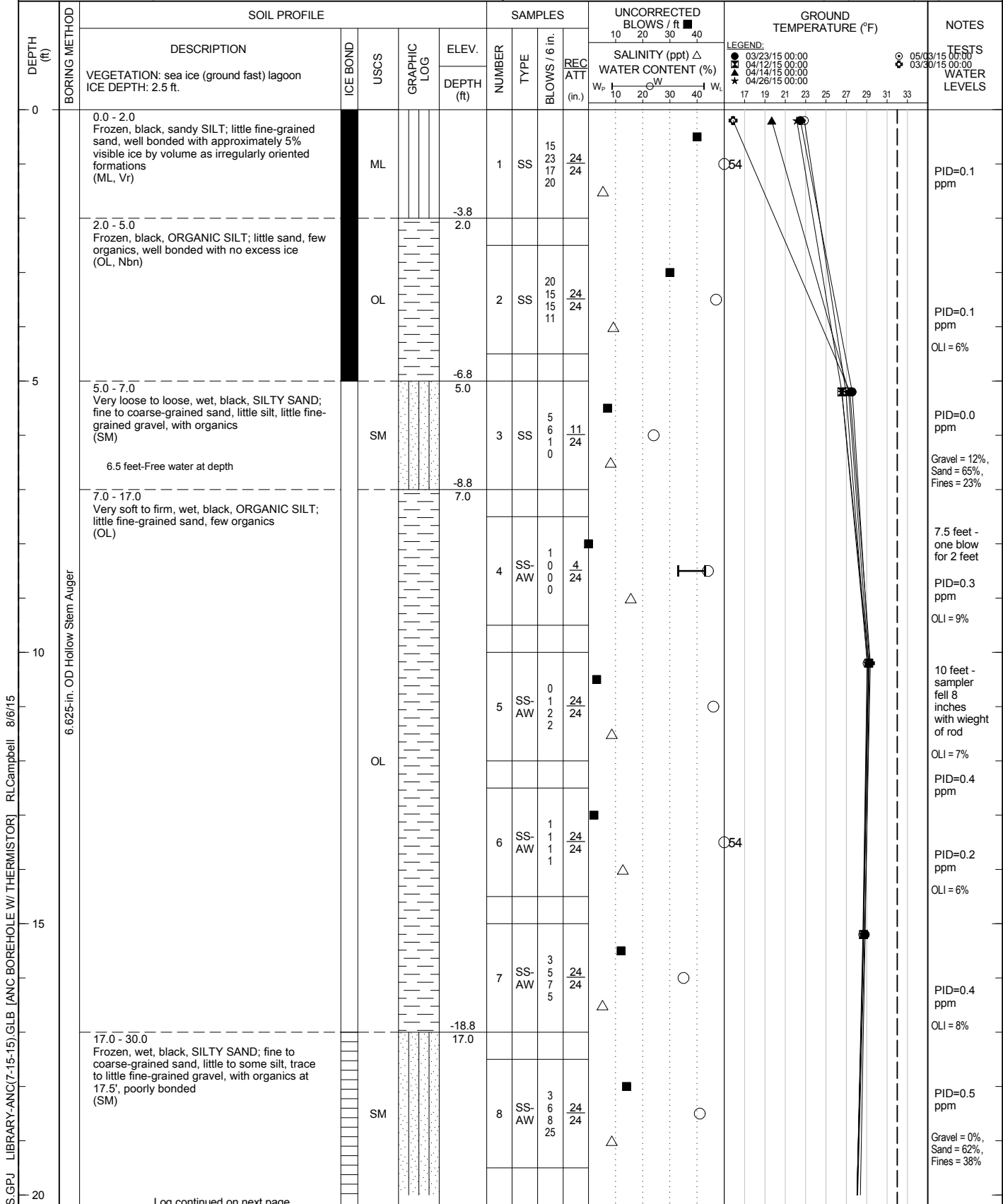
# RECORD OF BOREHOLE K15-06 (AP-44)

SHEET 1 of 2

PROJECT: Kivalina Causeway  
PROJECT NUMBER: 1419207  
LOCATION: Kivalina, AK

CLIENT: USACE  
DRILLING DATE: 3-21-15  
EQUIPMENT: Geoprobe 6712 DT

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -1.77 ft  
APPROX. COORDS: N: 1,844,699 E: 5,023,107



KIVALINA LOGS.GPJ LIBRARY-ANC(7-15-15).GLB [ANC BOREHOLE W/ THERMISTOR] RLCampbell 8/6/15



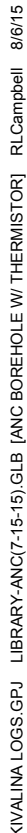
DEPTH SCALE: 1 inch to 2.5 feet  
DRILLING CONTRACTOR: Discovery Drilling Inc.  
DRILLER: Derek Dell

LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure A-8

## SHEET 2 of 2

DATUM: NAD83, AK State Plane Zone 8, NAVD-88  
APPROX. ELEVATION: -1.77 ft  
APPROX. COORDS: N: 1,844,699 E: 5,023,107



LOGGED: R. Campbell  
CHECKED: H. Weston  
CHECK DATE: 5/10/2015

Figure  
A-8

**APPENDIX B**  
**LABORATORY DATA**



## Testing Report Summary

Client	Golder Associates	Date Sample Recv'd	4/6/2015
Project	USACE Kivalina Causeway	W.O. #	34316
Location	See below	Lab #	Varies

All results will be posted to the website for your access and convenience. Samples will be kept for 30 days before being disposed. Please contact us if you would like the remaining material returned.

Lab ID	Sample ID	Test Performed	Test Method	Results
324	K15-01, Sample 15, Depth 52.5-54.5'	Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils	ASTM D4318	Liquid Limit ----
				Plastic Limit ----
				Plasticity Index Nonplastic
				USCS Silt
325	K15-02, Sample 11, Depth 0-2'			Liquid Limit ----
				Plastic Limit ----
				Plasticity Index Nonplastic
				USCS Silt
327	K15-02, Sample 3, Depth 5-7'			Liquid Limit ----
				Plastic Limit ----
				Plasticity Index Nonplastic
				USCS Silt
339	K15-03, Sample 1, Depth 0-1.5'			Liquid Limit ----
				Plastic Limit ----
				Plasticity Index Nonplastic
				USCS Silt
350	K15-04, Sample 1, Depth 1-2.5'			Liquid Limit ----
				Plastic Limit ----
				Plasticity Index Nonplastic
				USCS Silt
361	K15-05, Sample 2, Depth 2.5-4.5'			Liquid Limit ----
				Plastic Limit ----
				Plasticity Index Nonplastic
				USCS Silt
363	K15-05, Sample 4, Depth 7.5-9.5'			Liquid Limit 40
				Plastic Limit 33
				Plasticity Index 7
				USCS Silt or Organic Silt

continued on next page



## Testing Report Summary (cont'd)

Client	Golder Associates	Date Sample Recv'd	4/6/2015
Project	USACE Kivalina Causeway	W.O. #	34316
Location	See below	Lab #	Varies

Lab ID	Sample ID	Test Performed	Test Method	Results
371	K15-06, Sample 1, Depth 0-2'	Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils	ASTM D4318	Liquid Limit -
				Plastic Limit -
				Plasticity Index Nonplastic
				USCS Silt
374	K15-06, Sample 4, Depth 7.5-9.5'			Liquid Limit 43
				Plastic Limit 33
				Plasticity Index 10
				USCS Silt or Organic Silt
377	K15-06, Sample 7, Depth 15-17'			Liquid Limit ----
				Plastic Limit ----
				Plasticity Index Nonplastic
				USCS Silt

If you have questions regarding this summary report or the test procedures, please contact us.

*Maria*

Maria E. Kampsen, P.E.  
Laboratory Supervisor



## Testing Report Summary

Client	Golder Associates	Date Sample Recv'd	4/6/2015
Project	USACE Kivalina Causeway	W.O. #	34316
Location	Varies	Lab #	see below

All results will be posted to the website for your access and convenience. Samples will be kept for 30 days before being disposed. Please contact us if you would like the remaining material returned.

Sample ID	Test Performed	Test Method	Organic %
K15-01 Depth 47.5-49.5' (Lab No. 323)	Moisture, Ash & Organic Matter of Peat Materials	ASTM D2974	4.1
K15-02 Depth 25-27' (Lab No. 333)			5.1
K15-02 Depth 50-52' (Lab No. 338)			4.7
K15-04 Depth 22.5-24.5' (Lab No. 357)			4.0
K15-04 Depth 29.5-31.5' (Lab No. 359)			15.2
K15-06 Depth 2.5-4.5' (Lab No. 372)			5.8
K15-06 Depth 7.5-9.5' (Lab No. 374)			8.5
K15-06 Depth 10-12' (Lab No. 375)			6.5
K15-06 Depth 12.5-14.5' (Lab No. 376)			6.3
K15-06 Depth 15-17' (Lab No. 377)			7.5

*Maria*

Maria E. Kampsen, P.E.  
Laboratory Supervisor





# Visual Classification ASTM D-2488

## Test Summary Report

### Reporting Worksheet

Client Golder Associates  
 Project USACE Kivalina Causeway  
 Location Varies

Sample Date 4/6/2015  
 W.O.# 34316  
 Lab No. varies

Lab #	Boring		Depth		Percent			Grain			PI	USCS	Color	Free Water	Organics	Ice	Remarks	Moisture	
																		Wet	
	TH	SA	From (Feet)	To (Feet)	Gravel	Sand	#200	Max	Shape	Sand	Dry Str.								
310	K15-01	1	0	1.5	1	80	19	1/4"	-	M	M	NP	SM	Black		Trace		1.13	34.02
																		26.89	28
311	K15-01	2	2.5	4	0	80	20	S	-	M	M	NP	SM	Black		Trace		1.15	62.9
																		51.14	24
312	K15-01	3	5	6.5	5	80	15	3/8"	-	M	-	NP	SM	Black		Trace		1.16	20.8
																		16.15	31
313	K15-01	4	7.5	9	5	80	15	1/4"	-	M	M	NP	SM	Black		Trace		1.15	37.05
																		30.27	23
314	K15-01	5	10	11.5	0	81	19	S	-	M	L	NP	SM	Black		None		1.17	33.05
																		25.95	29
315	K15-01	6	12.5	14.5	0	85	15	S	-	M	L	NP	SM	Black		None		1.15	30.63
																		25.03	23
316	K15-01	7	15.0	17	0	85	15	1/4"	-	M	L	NP	SM	Black		None		1.17	26.99
																		21.42	28
317	K15-01	8	17.5	19.5	4	70	26	1/4"	-	M	L	NP	SM	Black		Trace		1.18	22.64
																		18.25	26
318	K15-01	9	22.5	24.5	0	85	15	1/4"	-	M	H	NP	SM	Black		None		1.15	24.74
																		20.12	24
319	K15-01	10	27.5	29.5	0	85	15	1/4"	-	M	L	NP	SM	Black		None		1.16	30.47
																		24.85	24
320	K15-01	11	32.5	34.5	4	48	48	1/4"	-	F/M	H	NP	SM	Black		None		1.15	26.62
																		21.17	27
321	K15-01	12	37.5	39.5	25	60	15	1"	-	F/M	L	NP	SM	Black		None		1.16	24.97
																		21.18	19
322	K15-01	13	42.5	44.5	36	56	8	1"	-	F/M	L	NP	SP-SM	Black		None		1.15	16.97
																		15.15	13
323	K15-01	14	47.5	49.5	15	35	50	1/2"	-	F/M	VH	M	CL	Gray		None		1.15	21.19
																		17.03	26
324	K15-01	15	52.5	54.5	0	5	95	S	-	F/M	H	NP	ML	Gray		None		1.17	17.62
																		13.69	31

Continued on next page



# Visual Classification ASTM D-2488

## Test Summary Report (cont'd)

### Reporting Worksheet

Client Golder Associates  
 Project USACE Kivalina Causeway  
 Location See below

Sample Date 4/6/2015  
 W.O.# 34316  
 Lab No. varies

Lab #	Boring		Depth		Percent			Grain			Dry Str.	PI	USCS	Color	Free Water	Organics	Ice	Remarks	Moisture	
																			Wet	
	TH	SA	From	To	Gravel	Sand	#200	Max	Shape	Sand			Symbol						Dry	%
325	K15-02	1	0	2	0	5	95	S	-	F	M	NP	ML	Black/Brown		None		1.16	15.88	63
																			10.19	
326	K15-02	2	2.5	4.5	0	20	80	S	-	F	H	NP	ML	Gray		None		1.15	20.15	34
																			15.36	
327	K15-02	3	5	7	5	87	8	1/4"	-	F/M	L	NP	SP-SM	Black		None		1.16	26.66	22
																			22.04	
328	K15-02	4	7.5	9.5	0	50	50	S	-	F	M	NP	ML	Black		None		1.13	20.09	36
																			15.1	
329	K15-02	5	10	12	0	75	25	S	-	F	L	NP	SM	Black		None		1.13	27.58	30
																			21.49	
330	K15-02	6	12.5	14.5	15	50	35	1/4"	-	F/M	L	NP	SM	Black		None		1.14	17.23	19
																			14.64	
331	K15-02	7	15.0	17	9	82	9	1/4"	-	F/M	L	NP	SP-SM	Black		None		1.14	36.65	19
																			31.08	
332	K15-02	8	20.0	22	1	69	30	S	-	F	L	NP	SM	Black		None		1.16	15.39	37
																			11.55	
333	K15-02	9	25	27	0	25	75	S	-	F	M	NP	ML	Black		None		1.17	24.07	42
																			17.32	
334	K15-02	10	30	32	24	59	17	F/C	-	F/M	L	NP	SM	Black		None		1.16	28.03	46
																			19.57	
335	K15-02	11	35	37	50	35	15	F/C	-	F/M	L	NP	GM	Black		None		1.15	30.79	12
																			27.68	
336	K15-02	12	40	42	41	51	8	F/C	-	F/M	L	NP	SW-SM	Black		None		1.17	23.74	11
																			21.5	
337	K15-02	13	45	47	20	30	50	F/C	-	F/M	H	NP	GM	Gray		None		1.17	29.56	31
																			22.83	
338	K15-02	14	50	52	0	5	95	S	-	M	VH	L	ML	Gray		None		1.17	21.73	26
																			17.47	
339	K15-03	1	0	1.5	0	15	85	S	-	M	M	NP	ML	Black/Brown		None		1.14	12.1	51
																			8.39	

Continued on next page



# Visual Classification ASTM D-2488

## Test Summary Report (cont'd)

### Reporting Worksheet

Client Golder Associates  
 Project USACE Kivalina Causeway  
 Location See below

Sample Date 4/6/2015  
 W.O.# 34316  
 Lab No. varies

Lab #	Boring		Depth		Percent			Grain			Dry Str.	PI	USCS	Color	Free Water	Organics	Ice	Remarks	Moisture	
																			Wet	
	TH	SA	From	To	Gravel	Sand	#200	Max	Shape	Sand			Symbol						Dry	%
340	K15-03	2	2.5	4.5	0	15	85	S	-	M	M	NP	ML	Black/Brown		None		1.16	27.26	38
																			20.07	
341	K15-03	3	5	7	5	75	20	1/4"	-	F/M	L	NP	SM	Black		None		1.15	38.15	22
																			31.43	
342	K15-03	4	7.5	9.5	9	83	8	1/4"	-	F/M	L	NP	SP-SM	Black		None		1.15	25.66	19
																			21.74	
343	K15-03	5	10	12	25	50	25	1/4"	-	F/M	L	NP	ML	Black/Brown		None		1.13	18.73	25
																			15.16	
344	K15-03	6	12.5	14.5	3	85	12	1/4"	-	F/M	L	NP	SP-SM	Black/Brown		None		1.13	17.41	21
																			14.57	
345	K15-03	7	15.0	17	5	80	15	1/4"	-	F/M	L	NP	SM	Brown		None		1.16	20.81	25
																			16.83	
346	K15-03	8	17.5	19.5	8	82	10	1/4"	-	F/M	L	NP	SW-SM	Black/Brown		None		1.16	14.7	20
																			12.48	
347	K15-03	9	22.5	24.5	10	60	30	1/2"	-	F/M	L	NP	SM	Black		None		1.14	15.65	28
																			12.47	
348	K15-03	10	27.5	29.5	6	64	30	1/4"	-	F/M	M	NP	SM	Black		None		1.16	23.5	25
																			19.1	
349	K15-03	11	29.5	31.5	1	80	19	S	-	S	M	NP	SM	Black		None		1.15	24.71	30
																			19.27	
350	K15-04	1	1	2.5	5	10	85	1/4"	-	S	H	L	ML	Black		None		1.16	29.4	30
																			22.93	
351	K15-04	2	3.5	5	5	75	20	1/4"	-	F/M	L	NP	SM	Black		None		1.14	28.47	53
																			19.06	
352	K15-04	3	6	7.5	1	91	10	1/4"	-	F/M	L	NP	SP-SM	Black		None		1.16	13.32	24
																			10.98	
353	K15-04	4	8.5	10	9	85	6	3/58"	-	F/M	L	NP	SP-SM	Black		None		1.15	17.47	20
																			14.76	
354	K15-04	5	12.5	14.5	10	85	5	1/4"	-	F/M	L	NP	SP	Black		None		1.15	19.41	17
																			16.7	

Continued on next page



# Visual Classification ASTM D-2488

## Test Summary Report (cont'd)

### Reporting Worksheet

Client Golder Associates  
 Project USACE Kivalina Causeway  
 Location See below

Sample Date 4/6/2015  
 W.O.# 34316  
 Lab No. varies

Lab #	Boring		Depth		Percent			Grain			Dry Str.	PI	USCS	Color	Free Water	Organics	Ice	Remarks	Moisture	
																			Wet	
	TH	SA	From	To	Gravel	Sand	#200	Max	Shape	Sand			Symbol						Dry	%
355	K15-04	6	15	17	12	77	11	1/2"	-	F/M	L	NP	SW-SM	Brown		None		1.14	20.96	17
																			18.05	
356	K15-04	7	17.5	19	15	80	5	3/8"	-	F/M	L	NP	SP	Black		None		1.15	15.25	15
																			13.41	
357	K15-04	8	22.5	24.5	4	72	24	3/8"	-	F/M	M	NP	SM	Black		None		1.14	27.36	23
																			22.51	
358	K15-04	9	27.5	29.5	0	5	95	S	-	M	H	NP	ML	Black		None		1.16	23.93	45
																			16.88	
359	K15-04	10	29.5	31.5	0	5	95	S	-	M	M	NP	ML	Black		Trace		1.15	14.29	40
																			10.53	
360	K15-05	1	0.0	1.5	1	74	25	S	-	M	L	NP	SM	Black		Trace		1.15	15.66	38
																			11.64	
361	K15-05	2	2.5	4.5	0	5	95	S	-	M	H	L	ML	Gray		None		1.15	23.34	32
																			17.99	
362	K15-05	3	5.0	7	0	5	95	S	-	M	M	L	ML	Gray		None		1.17	21.48	42
																			15.52	
363	K15-05	4	7.5	9.5	0	5	95	S	-	M	VH	L	ML	Gray		None		1.15	31.72	37
																			23.43	
364	K15-05	5	10	12	0	69	31	S	-	M	L	NP	SM	Black		None		1.15	30.72	27
																			24.39	
365	K15-05	6	12.5	14.5	10	50	40	3/4"	-	F/M	M	NP	SM	Black		None		1.15	18.49	25
																			15.05	
366	K15-05	7	15	17	20	40	40	1/4"	-	F/M	L	NP	SM	Brown		None		1.15	26.53	24
																			21.69	
367	K15-05	8	17.5	19.5	16	67	17	1/4"	-	F/M	L	NP	SM	Brown		None		1.14	24.16	22
																			19.98	
368	K15-05	9	22.5	24.5	0	50	50	S	-	M	M	NP	ML	Black		None		1.16	17.12	29
																			13.5	
369	K15-05	10	27.5	28.1	38	47	15	1"	-	F/M	H	NP	SM	Black		None		1.15	20.45	18
																			17.56	

Continued on next page



# Visual Classification ASTM D-2488 Test Summary Report

## Reporting Worksheet

Client Golder Associates  
 Project USACE Kivalina Causeway  
 Location See below

Sample Date 4/6/2015  
 W.O.# 34316  
 Lab No. varies

Lab #	Boring		Depth		Percent			Grain			Dry Str.	PI	USCS Symbol	Color	Free Water	Organics	Ice	Remarks	Moisture	
																			Wet	
	TH	SA	From	To	Gravel	Sand	#200	Max	Shape	Sand									Dry	%
370	K15-05	11	30	30.5	46	48	6	3/4"	-	M	L	NP	SP-SM	Brown		None		1.14	20	11
																			18.07	
371	K15-06	1	0	2	0	5	95	S	-	M	M	NP	ML	Black		None		1.14	13.72	54
																			9.31	
372	K15-06	2	2.5	4.5	0	5	95	S	-	M	L	NP	ML	Black		None		1.14	18.6	47
																			12.98	
373	K15-06	3	5	7	12	65	23	1/4"	-	F/M	M	NP	SM	Black		None		1.16	34.69	24
																			28.22	
374	K15-06	4	7.5	9.5	0	5	95	S	-	M	H	L	ML	Gray		None		1.16	22.33	44
																			15.83	
375	K15-06	5	10.0	12	0	5	95	S	-	M	VH	L	ML	Gray		None		1.15	15.97	46
																			11.33	
376	K15-06	6	12.5	14.5	0	5	95	S	-	M	VH	L	ML	Gray		None		1.13	14.89	54
																			10.09	
377	K15-06	7	15.0	17	0	5	95	S	-	M	H	NP	ML	Gray		None		1.16	18.93	35
																			14.31	
378	K15-06	8	17.5	19.5	0	62	38	S	-	M	L	NP	SM	Black		None		1.15	22.34	41
																			16.15	
379	K15-06	9	22.5	24.5	5	75	20	1/4"	-	F/M	L	NP	SM	Black/Brown		None		1.17	11.07	30
																			8.78	
380	K15-06	10	27.5	28.3	11	64	25	3/8"	-	F/M	L	NP	SM	Black		None		1.14	21.45	30
																			16.82	
381	K15-06	11	30	31	55	41	4	1"	-	F/M	L	NP	GW	Brown		None		1.14	11.26	6
																			10.66	

If you have questions regarding this summary report or the test procedures, please contact us.

*Maria*

Maria E. Kampsen, P.E.  
 Laboratory Supervisor



# Conductivity Report Summary

Date Sample Recv'd 6/9/2014

Client	Golder Associates	W.O. #	33956
Project	USACE Kivalina Causeway	Lab #	Varies
Location	See below		

Lab ID	Sample ID	Test Performed	Test Method	Parts Per Thousand (ppt)
339	K15-03, Sample 1, 0'-1.5'	Conductivity	In House Procedure	4.5
340	K15-03, Sample 2, 2.5'-4.5'			2.3
341	K15-03, Sample 3, 5'-7'			3.3
342	K15-03, Sample 4, 7.5'-9'			2.7
343	K15-03, Sample 5, 10'-12'			4.9
344	K15-03, Sample 6, 12.5'-14.5'			3.9
345	K15-03, Sample 1, 15'-17'			4.4
346	K15-03, Sample 1, 17.5'-19.5'			5.5
347	K15-03, Sample 9, 22.5'-24.5'			4.9
348	K15-03, Sample 10, 27.5'-29.5'			8.4
349	K15-03, Sample 11, 29.5'-31.5'			8.0
371	K15-06, Sample 1, 0'-2'			5.3
372	K15-06, Sample 2, 2.5'-4.5'			9.2
373	K15-06, Sample 3, 5'-7'			8.2
374	K15-06, Sample 4, 7.5'-9.5'			15.6
375	K15-06, Sample 5, 10'-12'			8.6
376	K15-06, Sample 6, 12.5'-14.5'			12.7
377	K15-06, Sample 7, 15'-17'			5.2
378	K15-06, Sample 8, 17.5'-19.5'			8.6
379	K15-06, Sample 9, 22.5'-24.5'			7.1

continued on next page



## Conductivity Report Summary (cont'd)

Client	Golder Associates	Date Sample Recv'd	6/9/2014
Project	USACE Kivalina Causeway	W.O. #	33956
Location	See below	Lab #	Varies

Lab ID	Sample ID	Test Performed	Test Method	Parts Per Thousand (ppt)
380	K15-06, Sample 10, 27.5'-28.3'	Conductivity	In House Procedure	7.8
381	K15-06, Sample 11, 30'-31'			10.8

If you have questions regarding this summary report or the test procedures, please contact us.

*Maria*

Maria E. Kampsen, P.E.  
Laboratory Supervisor



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-01  
 Sample 1  
 Depth 0'-1.5'

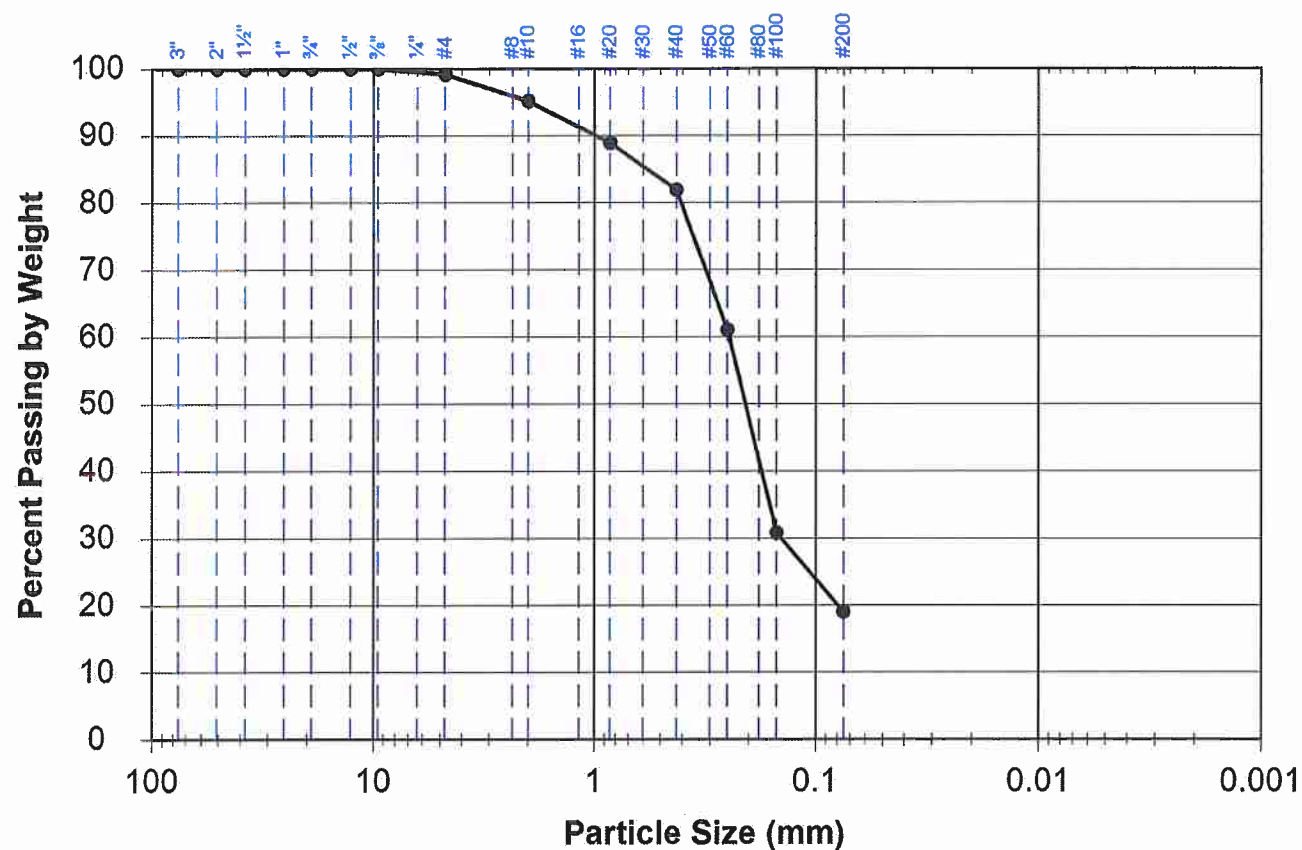
Lab Number 2015-310

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1 1/2"	100%	
--------	------	--

1"	100%	
----	------	--

3/4"	100%	
------	------	--

1/2"	100%	
------	------	--

3/8"	100%	
------	------	--

#4	99%	
----	-----	--

Total Weight of Sample 725g

#10	95%	
-----	-----	--

#20	89%	
-----	-----	--

#40	82%	
-----	-----	--

#60	61%	
-----	-----	--

#100	31%	
------	-----	--

#200	19.1%	
------	-------	--

Total Weight of Fine Fraction 307.6g





Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-01  
 Sample 5  
 Depth 10'-11.5'

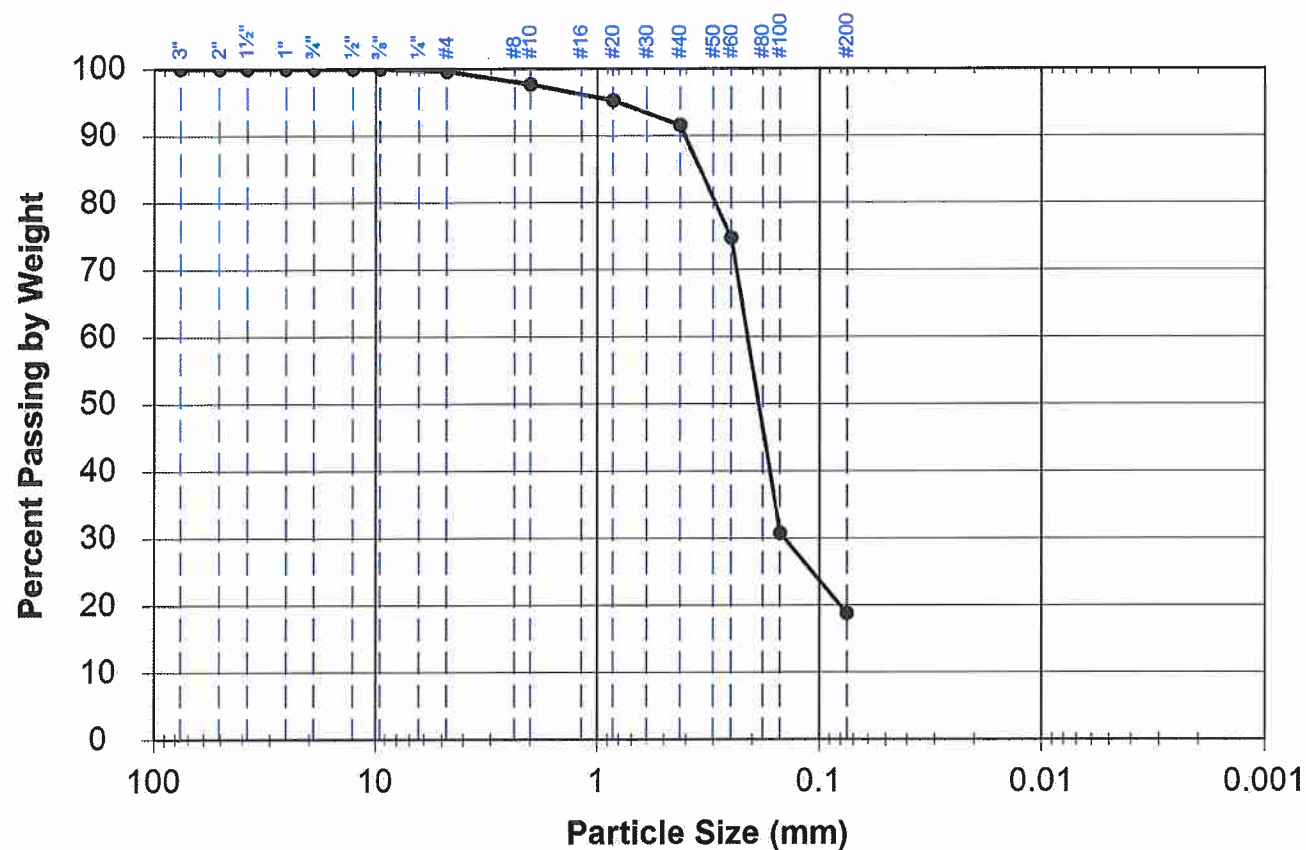
Lab Number 2015-314

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1 1/2"	100%	
--------	------	--

1"	100%	
----	------	--

3/4"	100%	
------	------	--

1/2"	100%	
------	------	--

3/8"	100%	
------	------	--

#4	100%	
----	------	--

Total Weight of Sample 292.5g

#10	98%	
-----	-----	--

#20	95%	
-----	-----	--

#40	92%	
-----	-----	--

#60	75%	
-----	-----	--

#100	31%	
------	-----	--

#200	18.8%	
------	-------	--

Total Weight of Fine Fraction 291.4g



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-01  
 Sample 8  
 Depth 17.5'-19.5'

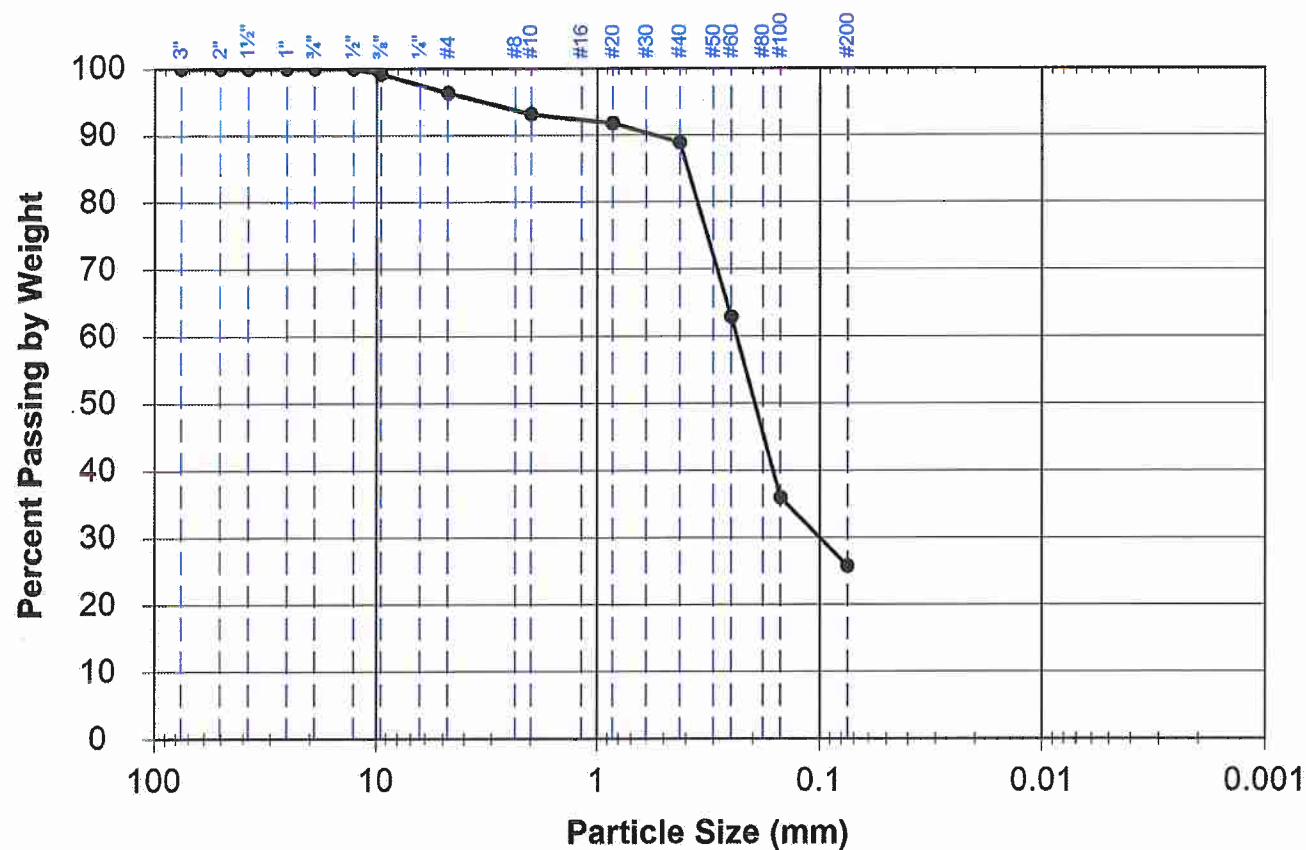
Lab Number 2015-317

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1 1/2"	100%	
--------	------	--

1"	100%	
----	------	--

3/4"	100%	
------	------	--

1/2"	100%	
------	------	--

3/8"	99%	
------	-----	--

#4	96%	
----	-----	--

Total Weight of Sample 465.9g

#10	93%	
-----	-----	--

#20	92%	
-----	-----	--

#40	89%	
-----	-----	--

#60	63%	
-----	-----	--

#100	36%	
------	-----	--

#200	25.8%	
------	-------	--

Total Weight of Fine Fraction 448.9g



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-01  
 Sample 11  
 Depth 32.5'-34.5'

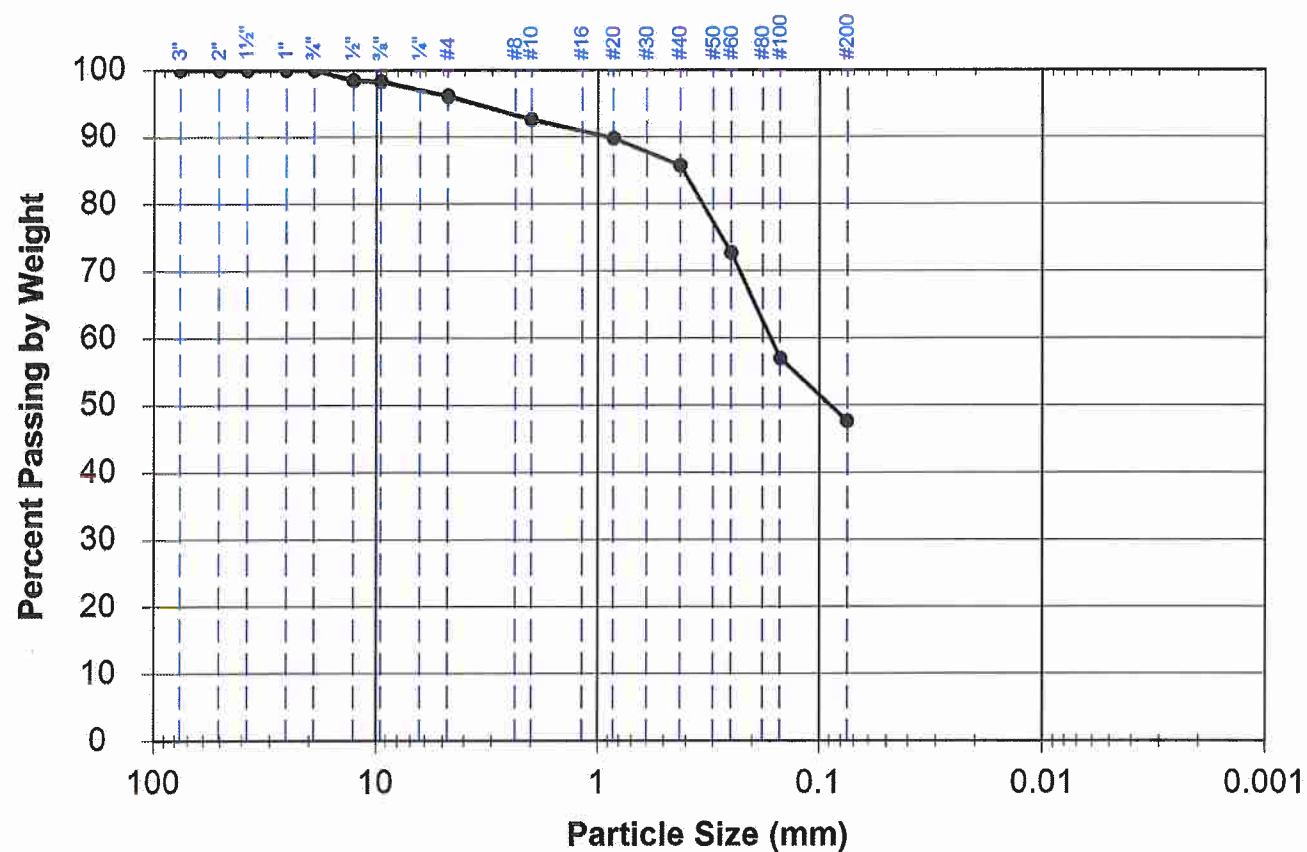
Lab Number 2015-320

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1½"	100%	
-----	------	--

1"	100%	
----	------	--

¾"	100%	
----	------	--

½"	98%	
----	-----	--

¾"	98%	
----	-----	--

#4	96%	
----	-----	--

Total Weight of Sample 772.7g		
-------------------------------	--	--

#10	93%	
-----	-----	--

#20	90%	
-----	-----	--

#40	86%	
-----	-----	--

#60	73%	
-----	-----	--

#100	57%	
------	-----	--

#200	47.6%	
------	-------	--

Total Weight of Fine Fraction 305.6g		
--------------------------------------	--	--



Client: Golder Associates Inc.  
Project: USACE Kivalina Causeway  
Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-01  
Sample 13  
Depth 42.5'-44.5'

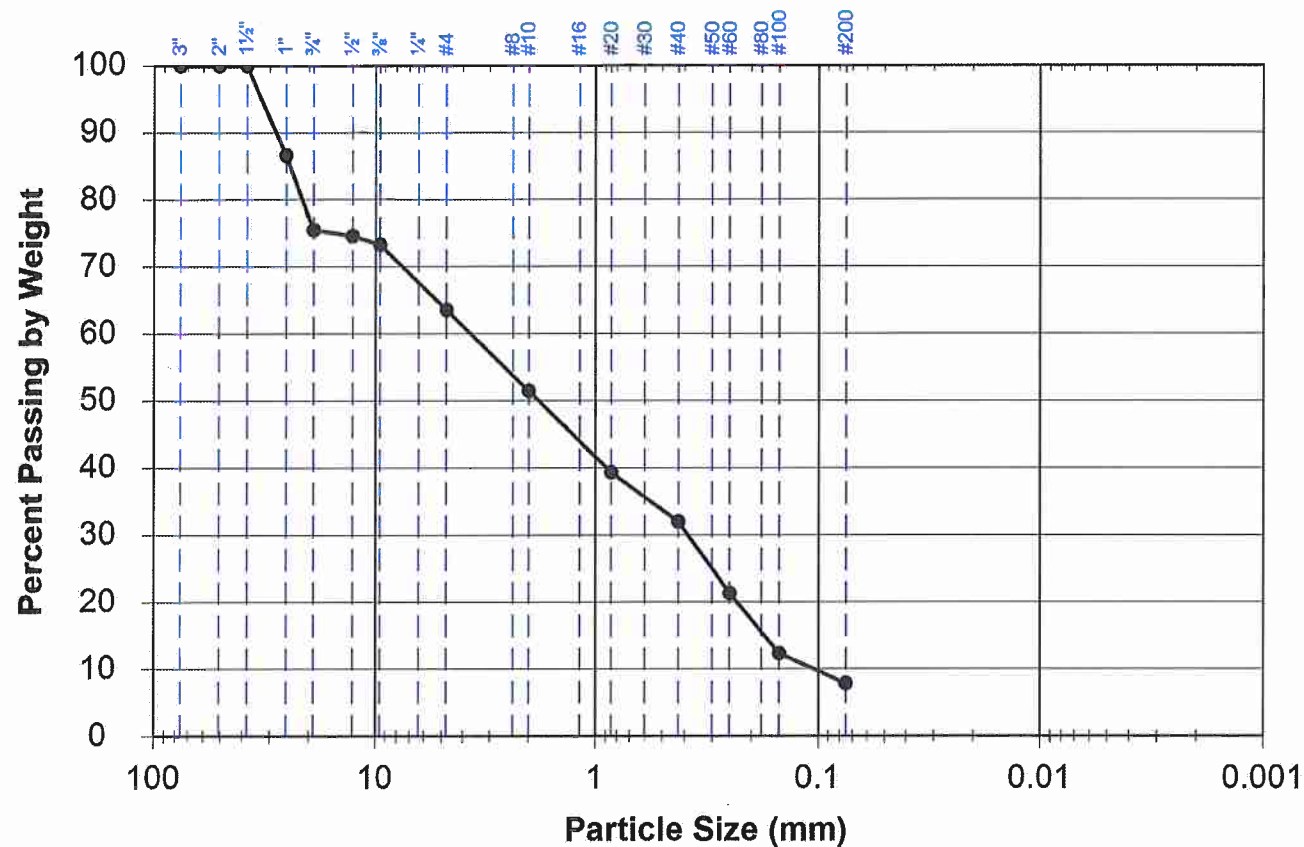
Lab Number 2015-322

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Poorly Graded Sand with Silt and Gravel, SP-SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	87%	
3/4"	75%	
1/2"	75%	
3/8"	73%	
#4	64%	
Total Weight of Sample 508.3g		
#10	51%	
#20	39%	
#40	32%	
#60	21%	
#100	12%	
#200	7.9%	
Total Weight of Fine Fraction 322.6g		







Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-02  
 Sample 5  
 Depth 10'-12'

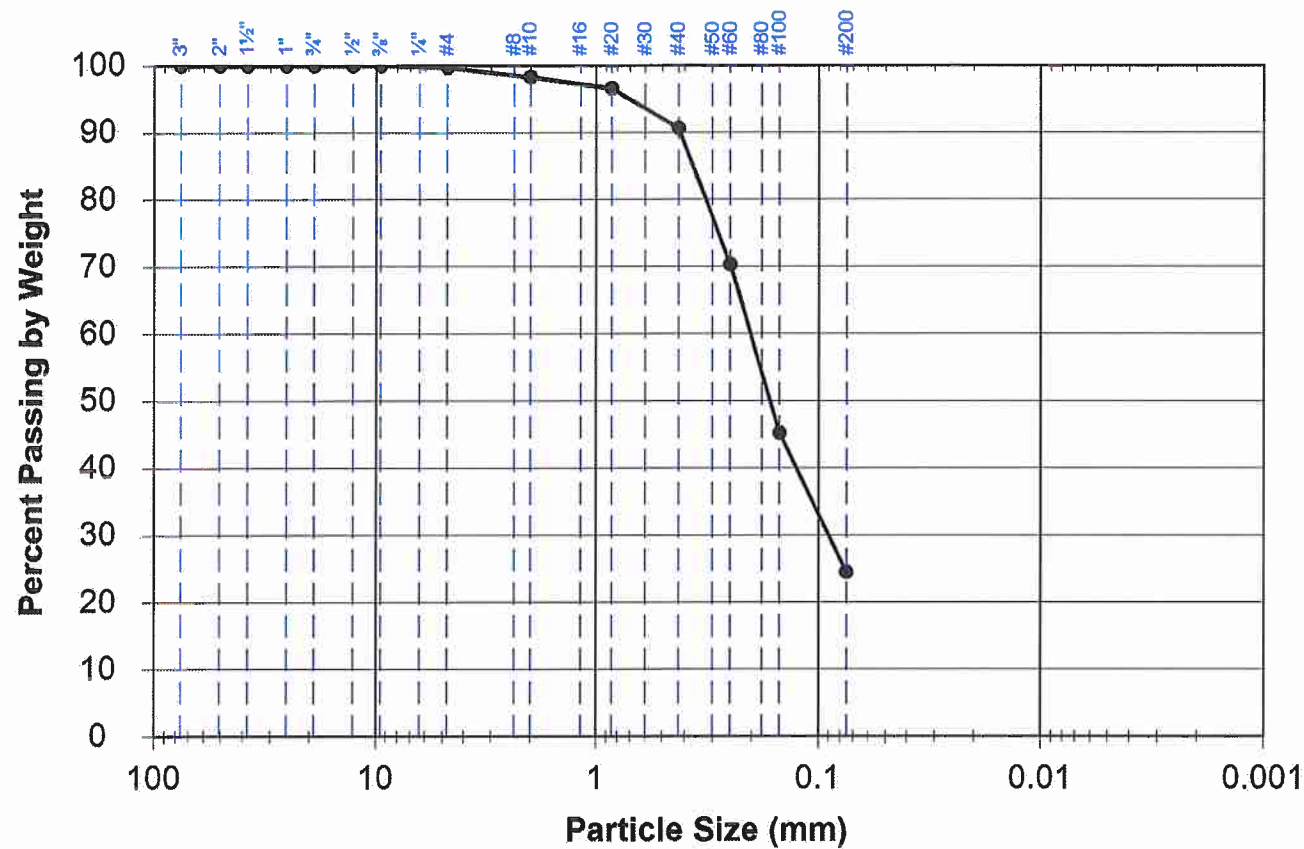
Lab Number 2015-329

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	100%	
⅜"	100%	
#4	100%	
Total Weight of Sample 537.6g		
#10	98%	
#20	97%	
#40	91%	
#60	70%	
#100	45%	
#200	24.5%	
Total Weight of Fine Fraction 535.5g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-02  
 Sample 7  
 Depth 15'-17'

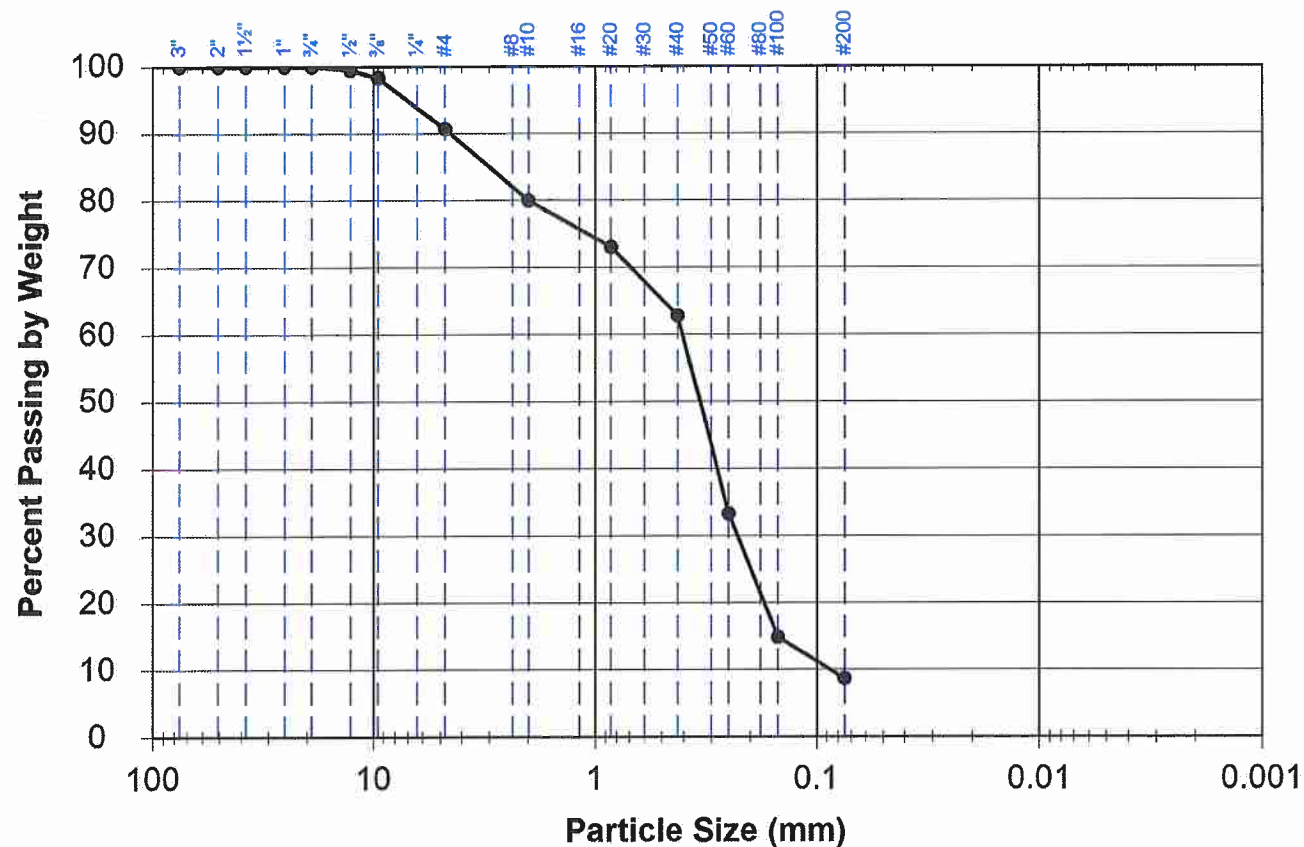
Lab Number 2015-331

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Poorly Graded Sand with Silt, SP-SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	100%	
3/8"	98%	
#4	91%	
Total Weight of Sample 553.7g		
#10	80%	
#20	73%	
#40	63%	
#60	33%	
#100	15%	
#200	8.7%	
Total Weight of Fine Fraction 501.5g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-02  
 Sample 8  
 Depth 20'-22'

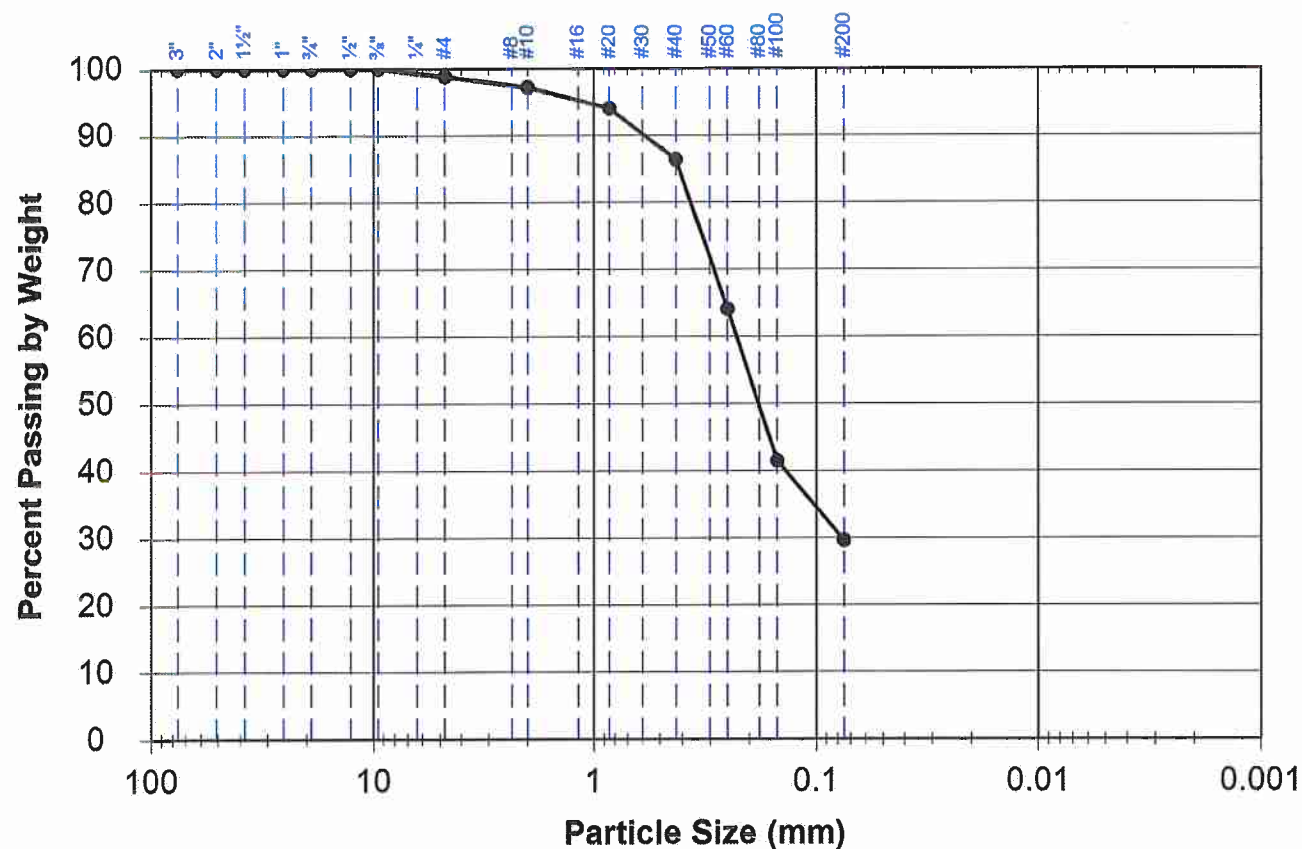
Lab Number 2015-332

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1½"	100%	
-----	------	--

1"	100%	
----	------	--

¾"	100%	
----	------	--

½"	100%	
----	------	--

⅜"	100%	
----	------	--

⅜"	100%	
----	------	--

#4	99%	
----	-----	--

Total Weight of Sample 213.3g

#10	97%	
-----	-----	--

#20	94%	
-----	-----	--

#40	86%	
-----	-----	--

#60	64%	
-----	-----	--

#100	41%	
------	-----	--

#200	29.7%	
------	-------	--

Total Weight of Fine Fraction 210.3g





Client: Golder Associates Inc.  
Project: USACE Kivalina Causeway  
Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-02  
Sample 10  
Depth 30'-32'

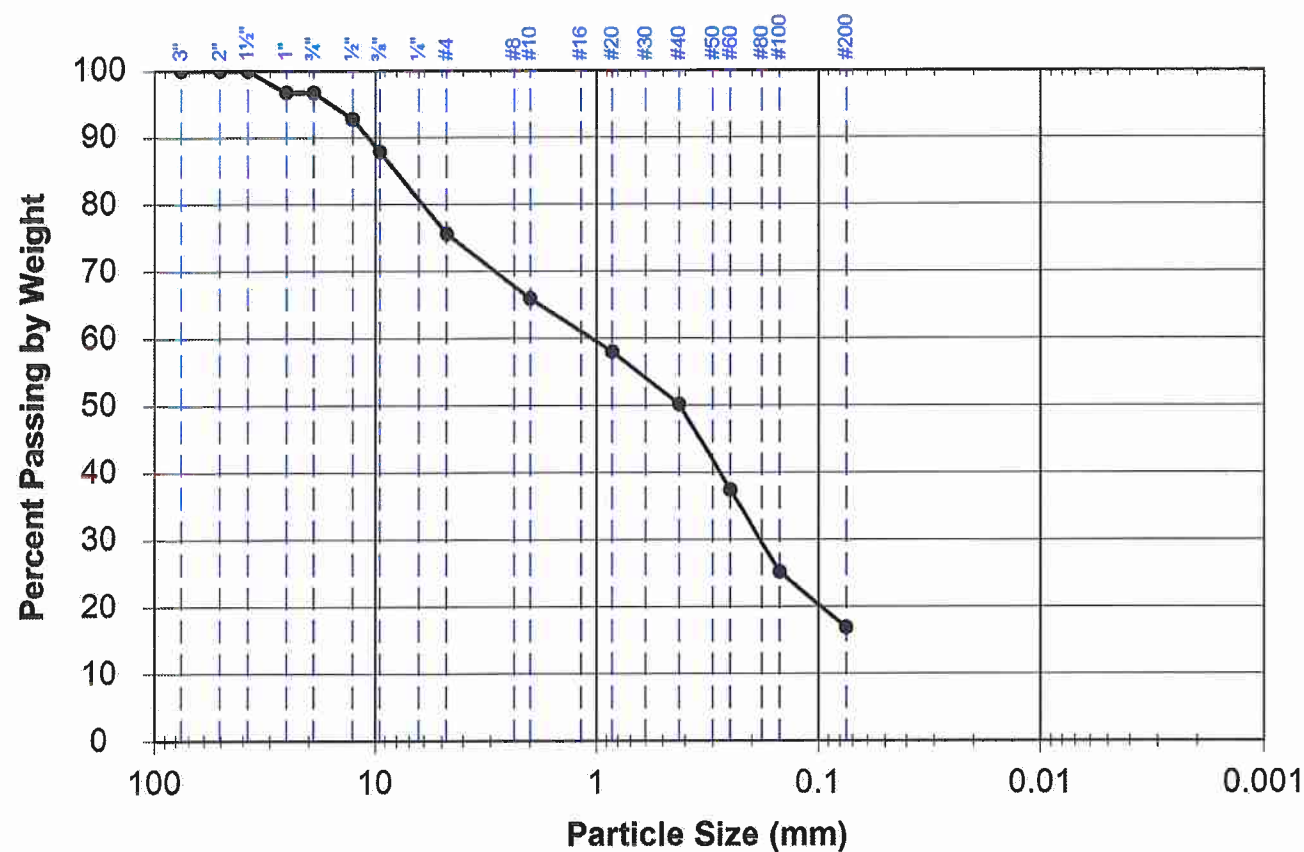
Lab Number 2015-334

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand with Gravel, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1½"	100%	
-----	------	--

1"	97%	
----	-----	--

¾"	97%	
----	-----	--

½"	93%	
----	-----	--

⅜"	88%	
----	-----	--

#4	76%	
----	-----	--

Total Weight of Sample 744.8g		
-------------------------------	--	--

#10	66%	
-----	-----	--

#20	58%	
-----	-----	--

#40	50%	
-----	-----	--

#60	37%	
-----	-----	--

#100	25%	
------	-----	--

#200	16.9%	
------	-------	--

Total Weight of Fine Fraction 561.7g		
--------------------------------------	--	--



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-02  
 Sample 12  
 Depth 40'-42'

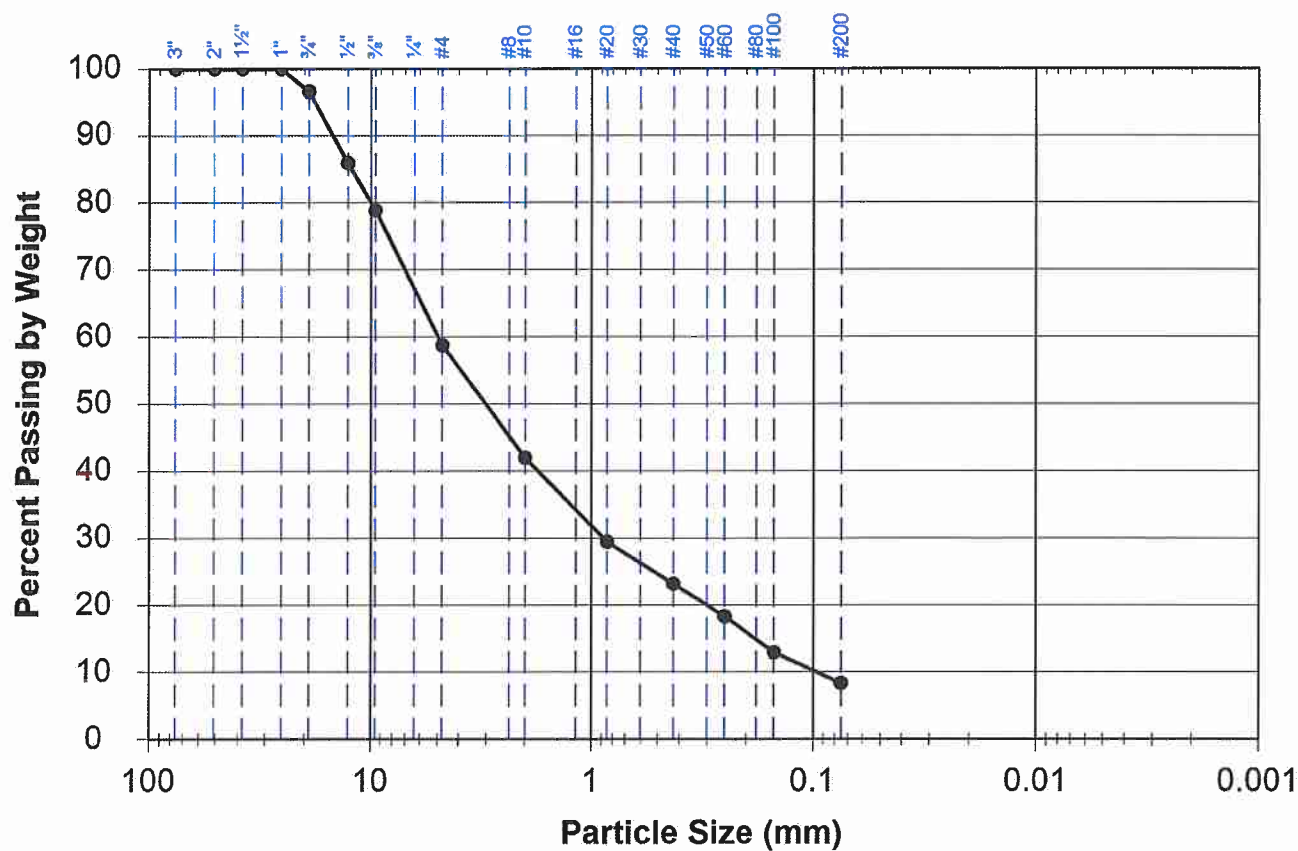
Lab Number 2015-336

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Well Graded Sand with Silt and Gravel, SW-SM

Frost Classification: Not Measured



Size Passing Specification

3" 100%

2" 100%

1 1/2" 100%

1" 100%

3/4" 97%

1/2" 86%

3/8" 79%

#4 59%

Total Weight of Sample 522.3g

#10 42%

#20 29%

#40 23%

#60 18%

#100 13%

#200 8.3%

Total Weight of Fine Fraction 306.4g



Client: Golder Associates Inc.  
Project: USACE Kivalina Causeway  
Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-03  
Sample 4  
Depth 7.5'-9.5'

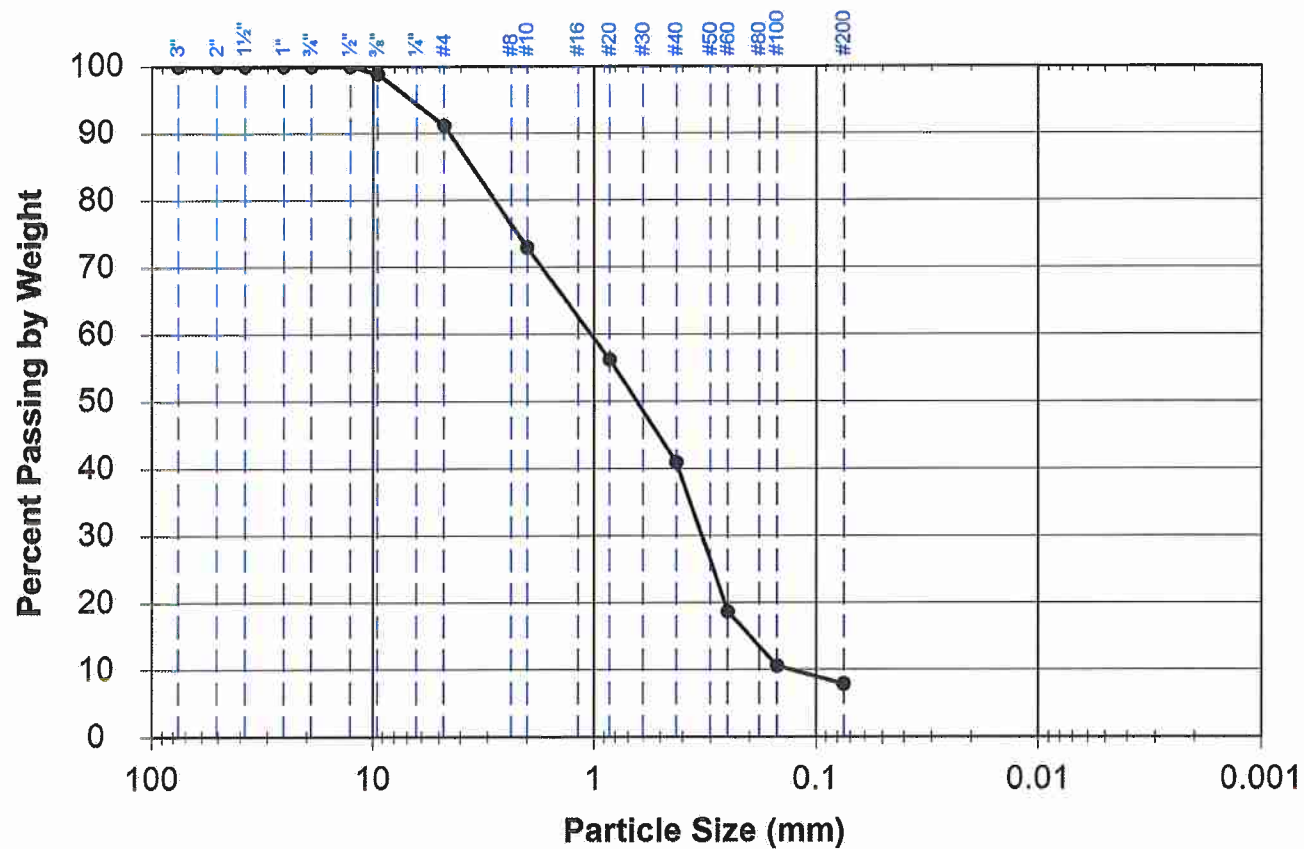
Lab Number 2015-342

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Poorly Graded Sand with Silt, SP-SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	100%	
3/8"	99%	
#4	91%	
Total Weight of Sample 614.1g		
#10	73%	
#20	56%	
#40	41%	
#60	19%	
#100	11%	
#200	7.9%	
Total Weight of Fine Fraction 558.6g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-03  
 Sample 6  
 Depth 12.5'-14.5'

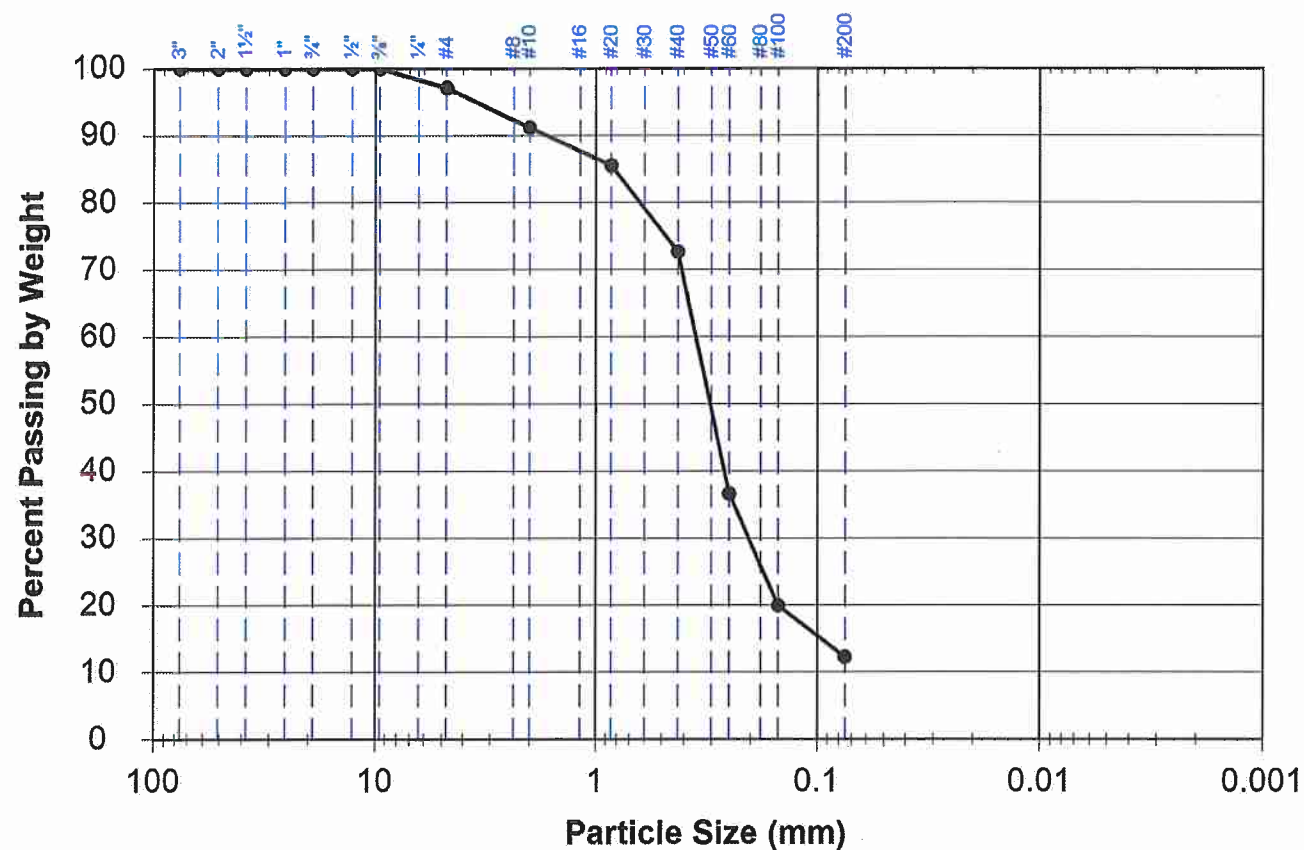
Lab Number 2015-344

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Poorly Graded Sand with Silt, SP-SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	100%	
3/8"	100%	
#4	97%	
Total Weight of Sample 537.3g		
#10	91%	
#20	85%	
#40	73%	
#60	37%	
#100	20%	
#200	12.3%	
Total Weight of Fine Fraction 521.3g		





Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-03  
 Sample 8  
 Depth 17.5-19.5'

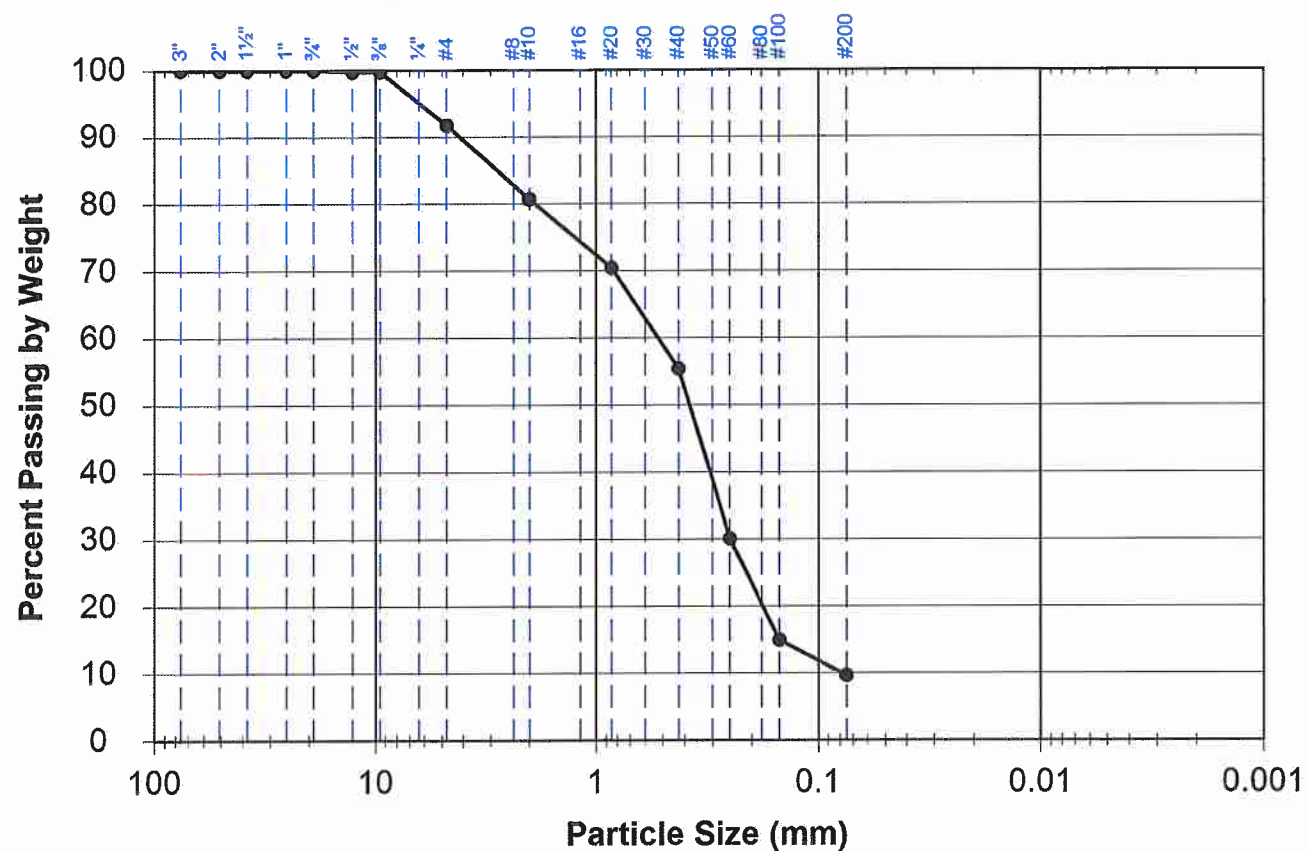
Lab Number 2015-346

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Well Graded Sand with Silt, SW-SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	100%	
⅜"	100%	
#4	92%	
Total Weight of Sample 741.3g		
#10	81%	
#20	70%	
#40	55%	
#60	30%	
#100	15%	
#200	9.7%	
Total Weight of Fine Fraction 378g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-03  
 Sample 10  
 Depth 27.5'-29.5'

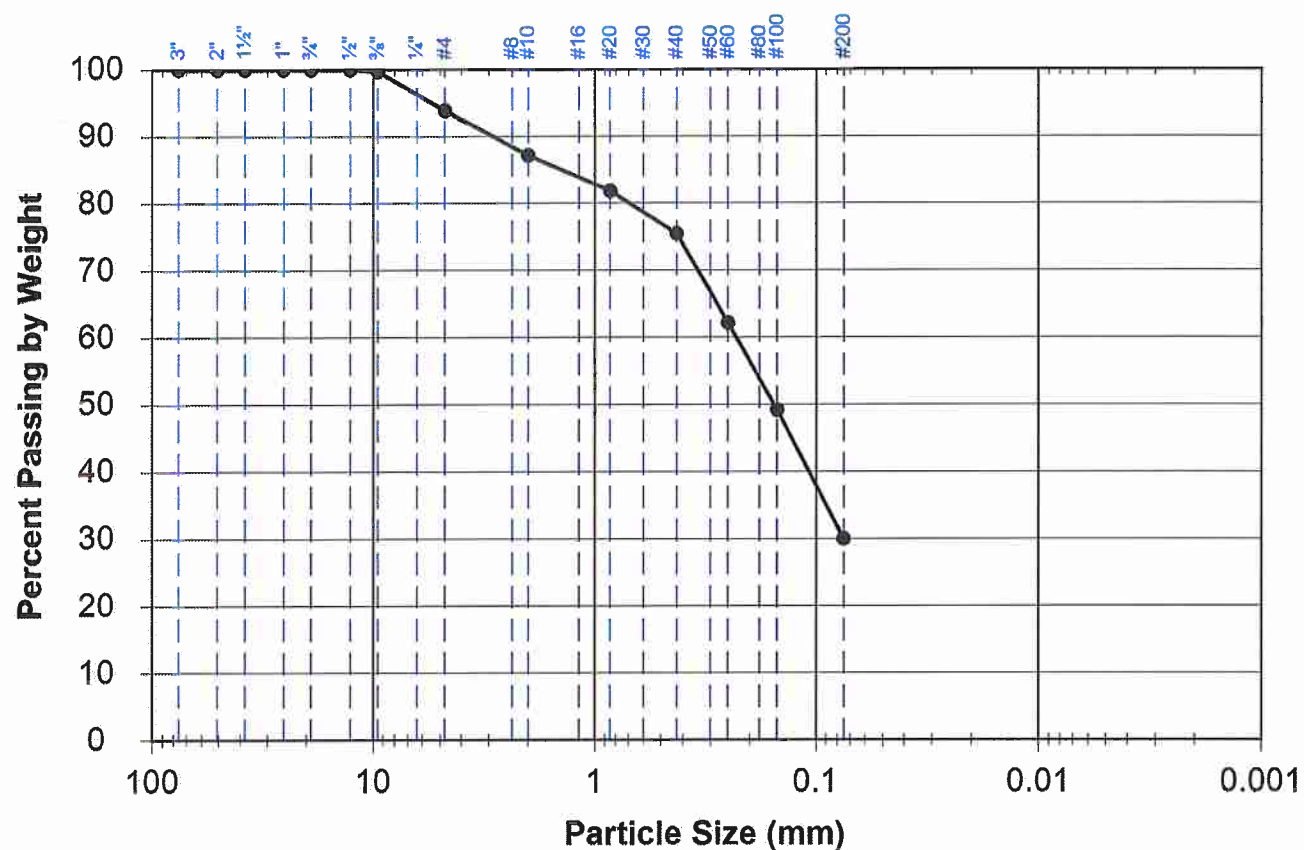
Lab Number 2015-348

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1 1/2"	100%	
--------	------	--

1"	100%	
----	------	--

3/4"	100%	
------	------	--

1/2"	100%	
------	------	--

3/8"	100%	
------	------	--

#4	94%	
----	-----	--

Total Weight of Sample 459.7g

#10	87%	
-----	-----	--

#20	82%	
-----	-----	--

#40	75%	
-----	-----	--

#60	62%	
-----	-----	--

#100	49%	
------	-----	--

#200	30.0%	
------	-------	--

Total Weight of Fine Fraction 430.9g



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-03  
 Sample 11  
 Depth 29.5'-31.5'

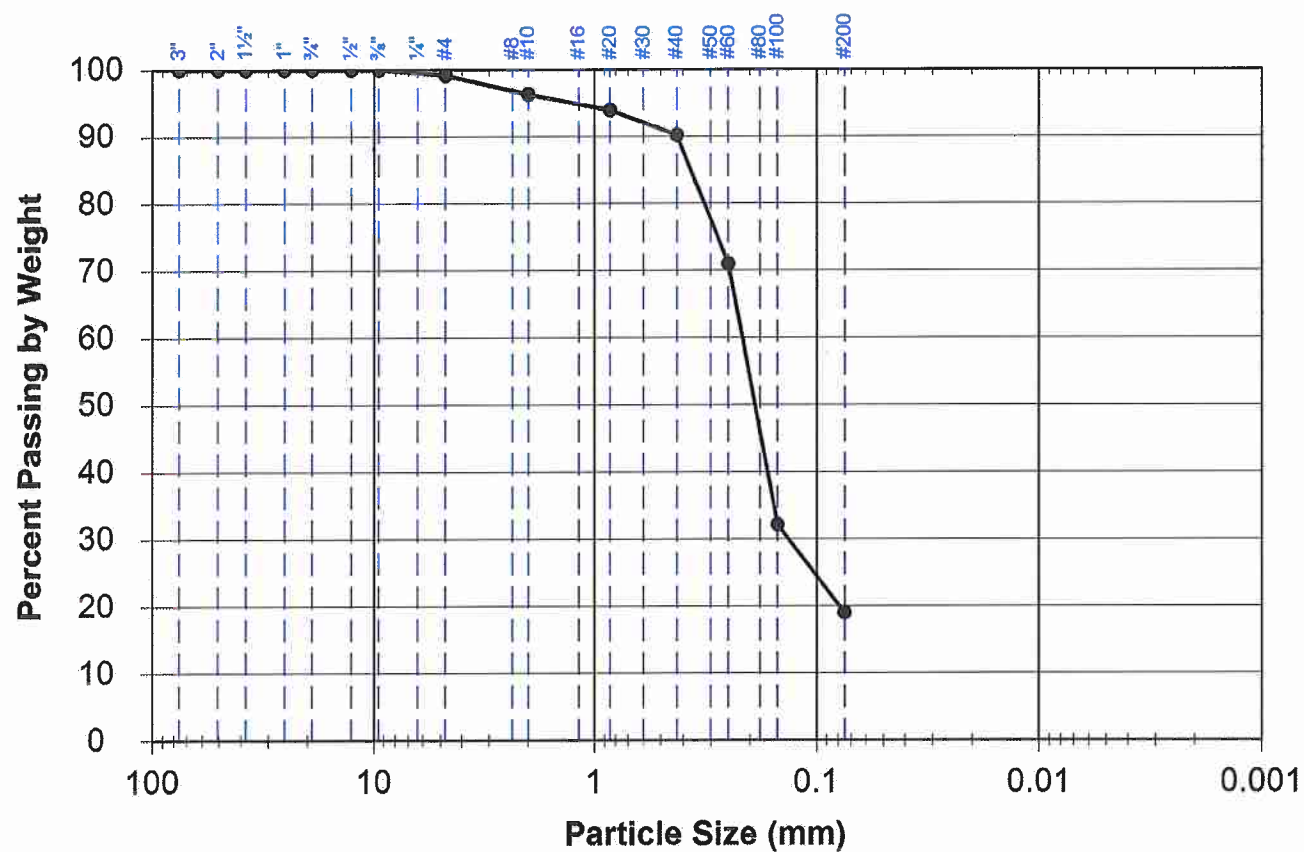
Lab Number 2015-349

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	100%	
⅜"	100%	
#4	99%	
Total Weight of Sample 525.1g		
#10	96%	
#20	94%	
#40	90%	
#60	71%	
#100	32%	
#200	19.0%	
Total Weight of Fine Fraction 519.9g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-04  
 Sample 2  
 Depth 3.5'-5'

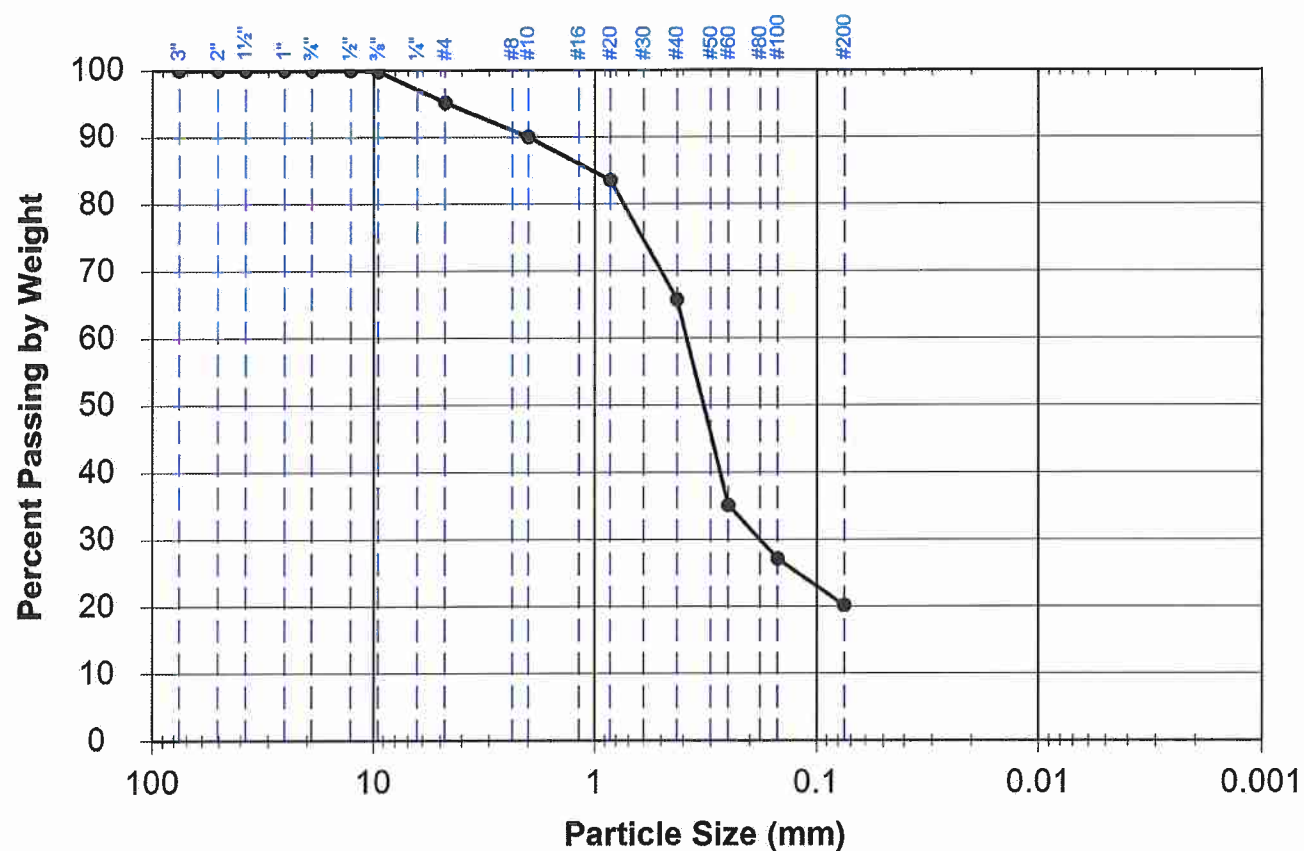
Lab Number 2015-351

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	100%	
⅜"	100%	
#4	95%	
Total Weight of Sample 918.7g		
#10	90%	
#20	84%	
#40	66%	
#60	35%	
#100	27%	
#200	20.2%	
Total Weight of Fine Fraction 392.4g		





Client: Golder Associates Inc.  
Project: USACE Kivalina Causeway  
Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-04  
Sample 3  
Depth 6'-7.5'

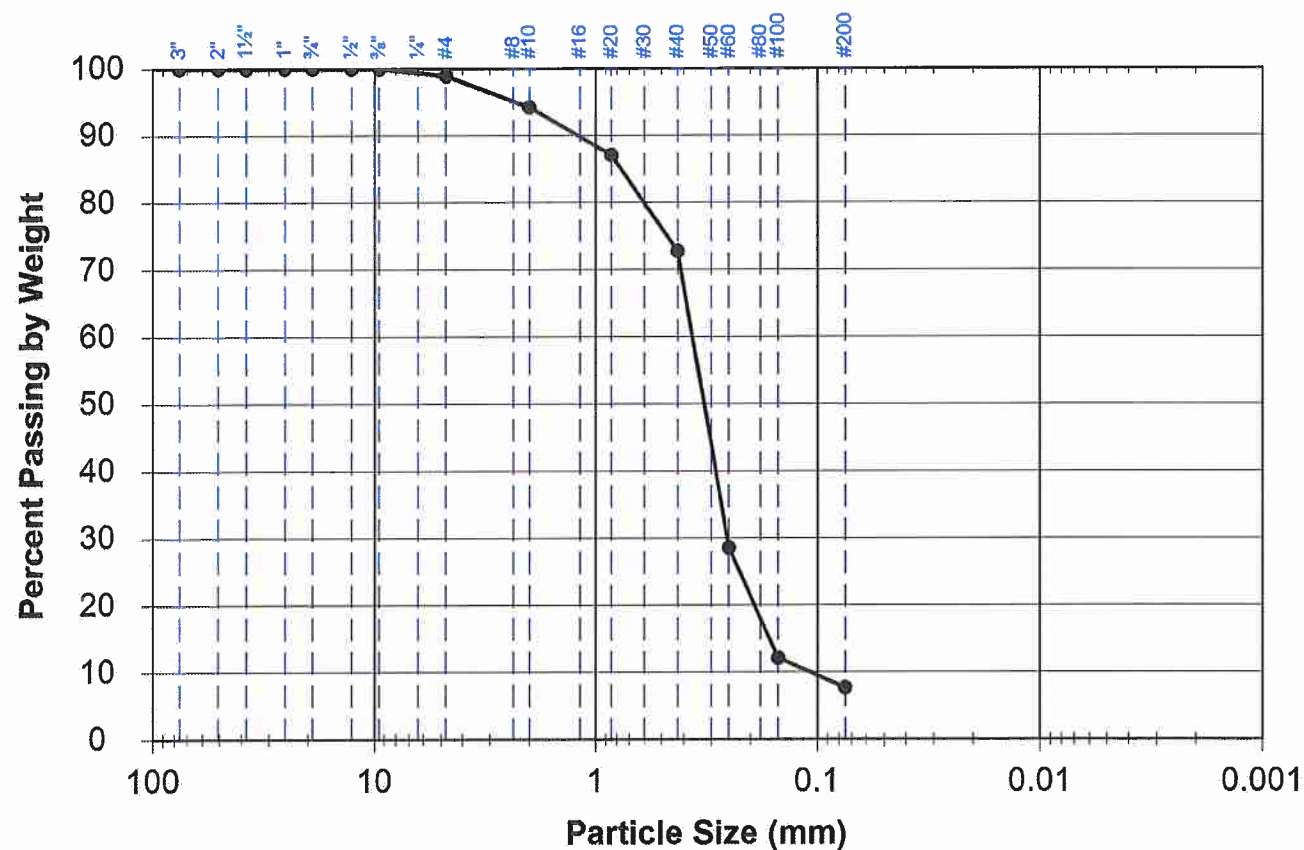
Lab Number 2015-352

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Poorly Graded Sand with Silt, SP-SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1 1/2"	100%	
--------	------	--

1"	100%	
----	------	--

3/4"	100%	
------	------	--

1/2"	100%	
------	------	--

3/8"	100%	
------	------	--

#4	99%	
----	-----	--

Total Weight of Sample 864.1g

#10	94%	
-----	-----	--

#20	87%	
-----	-----	--

#40	73%	
-----	-----	--

#60	29%	
-----	-----	--

#100	12%	
------	-----	--

#200	7.7%	
------	------	--

Total Weight of Fine Fraction 429.4g



Client: Golder Associates Inc.  
Project: USACE Kivalina Causeway  
Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-04  
Sample 4  
Depth 8.5'-10'

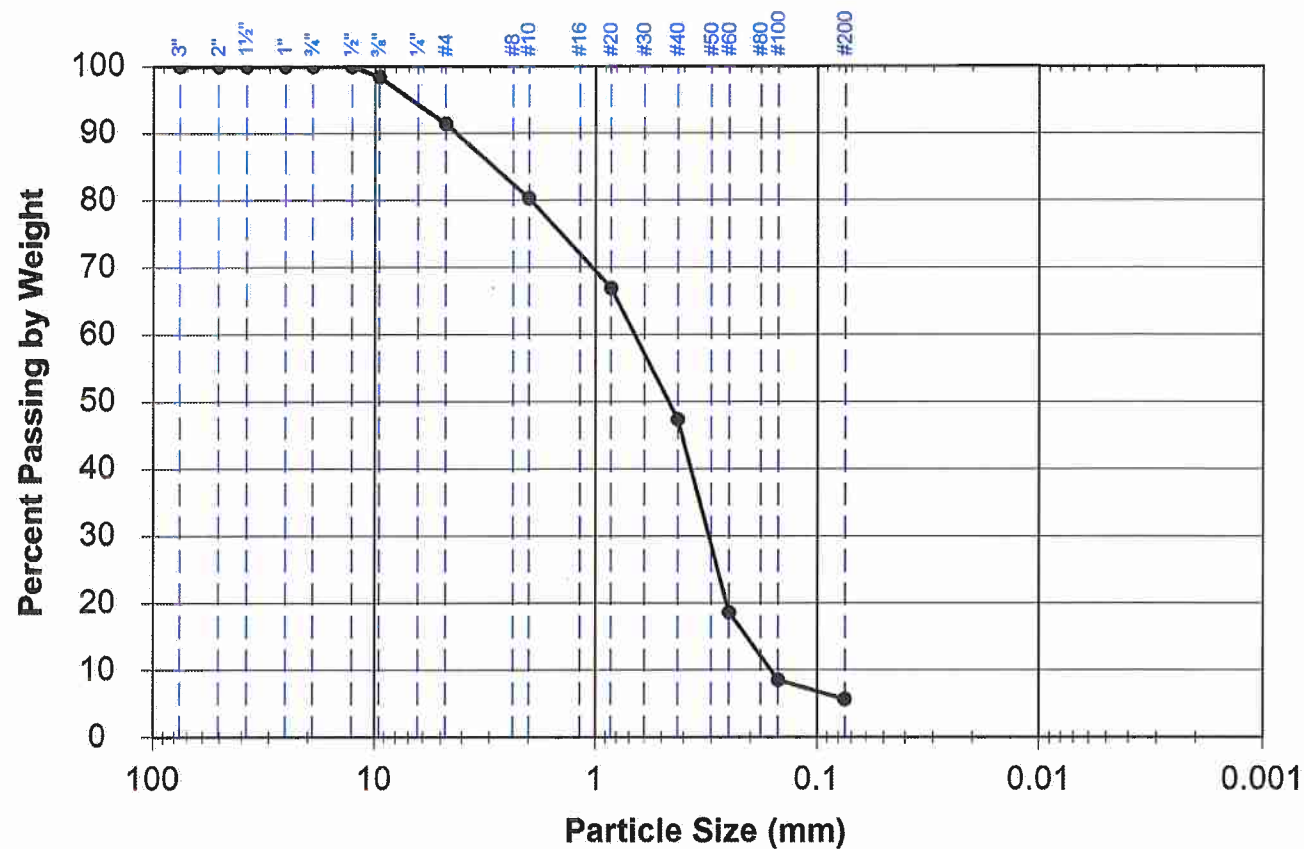
Lab Number 2015-353

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Poorly Graded Sand with Silt, SP-SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	100%	
3/8"	98%	
#4	91%	
Total Weight of Sample 1148.6g		
#10	80%	
#20	67%	
#40	47%	
#60	19%	
#100	9%	
#200	5.7%	
Total Weight of Fine Fraction 512.9g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-04  
 Sample 6  
 Depth 15'-17'

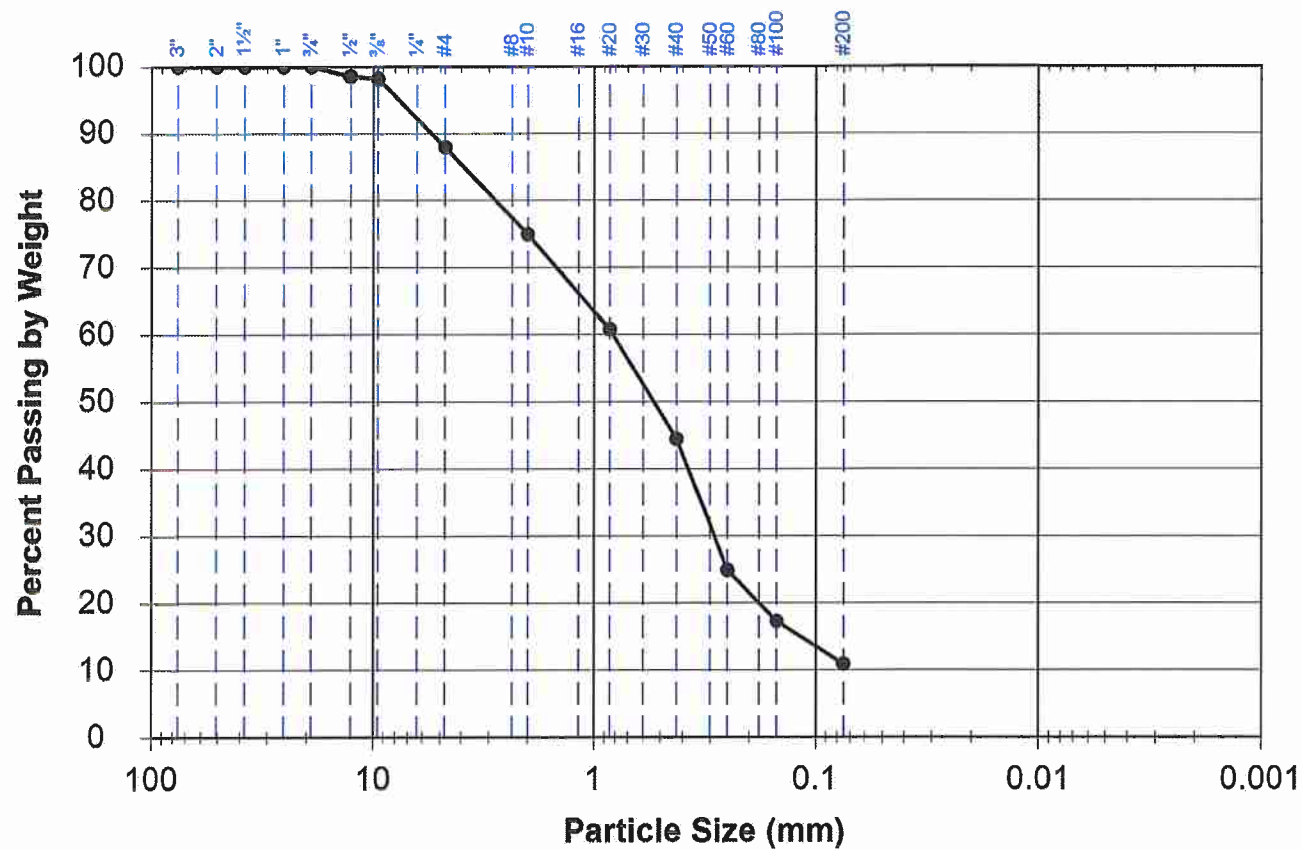
Lab Number 2015-355

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Well Graded Sand with Silt, SW-SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	99%	
⅜"	98%	
#4	88%	
Total Weight of Sample 539.4g		
#10	75%	
#20	61%	
#40	44%	
#60	25%	
#100	17%	
#200	10.9%	
Total Weight of Fine Fraction 473.3g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-04  
 Sample 8  
 Depth 22.5'-24.5'

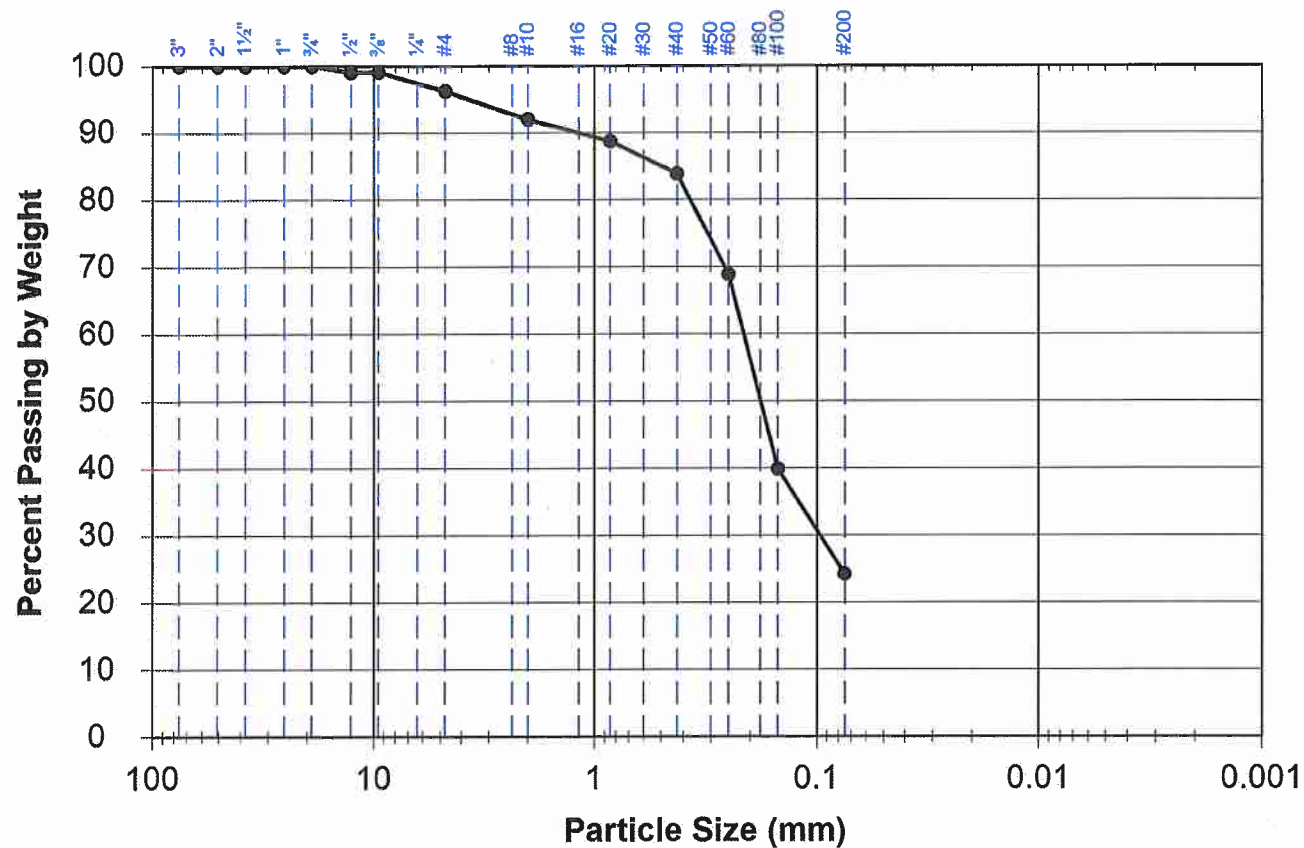
Lab Number 2015-357

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	99%	
3/8"	99%	
#4	96%	
Total Weight of Sample 365g		
#10	92%	
#20	89%	
#40	84%	
#60	69%	
#100	40%	
#200	24.3%	
Total Weight of Fine Fraction 351.6g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-05  
 Sample 1  
 Depth 0'-1.5'

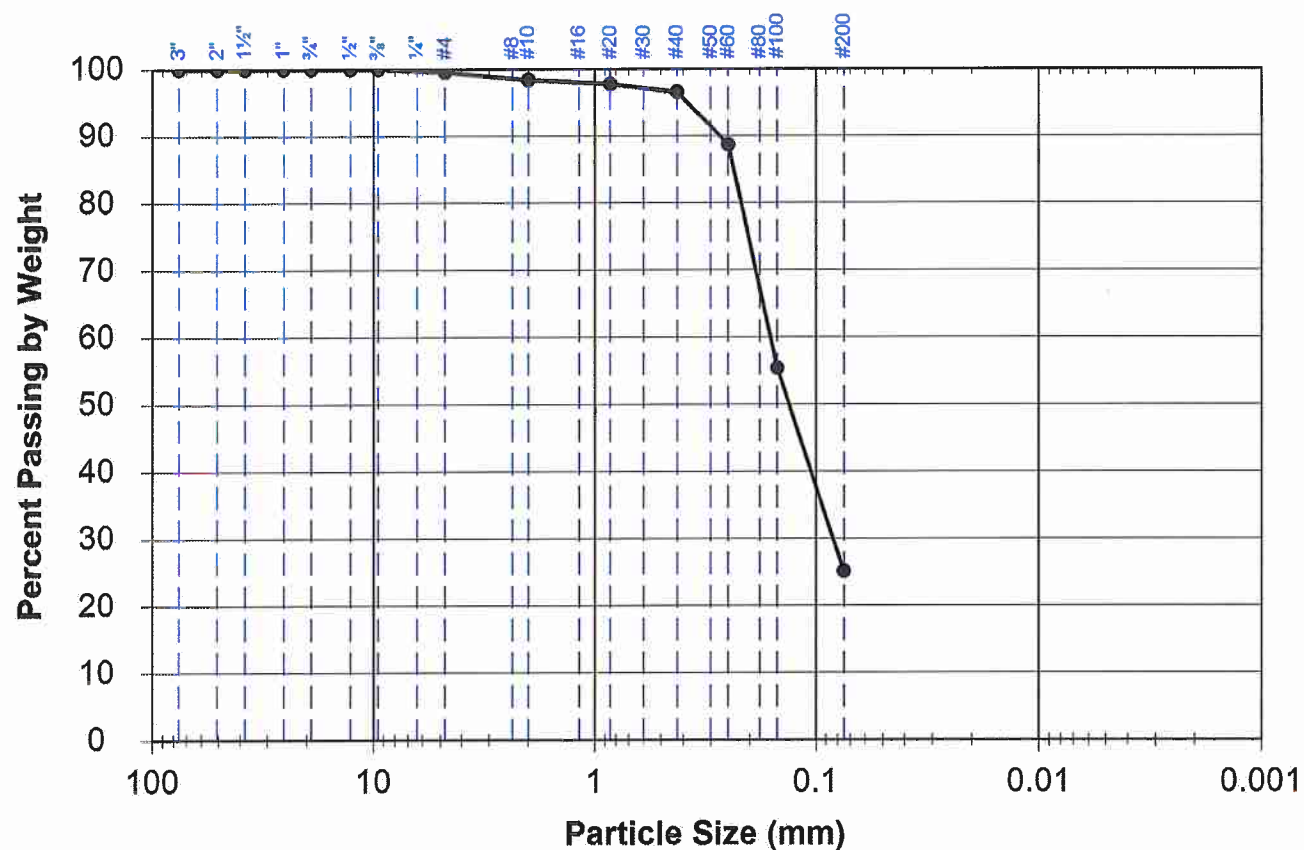
Lab Number 2015-360

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	100%	
3/8"	100%	
#4	99%	
Total Weight of Sample 339.9g		
#10	98%	
#20	98%	
#40	97%	
#60	89%	
#100	55%	
#200	25.2%	
Total Weight of Fine Fraction 338.2g		





**Client:** Golder Associates Inc.  
**Project:** USACE Kivalina Causeway  
**Work Order:** A34316

## Particle Size Distribution

ASTM D422

**Location:** Test Borehole K15-05  
 Sample 5  
 Depth 10'-12'

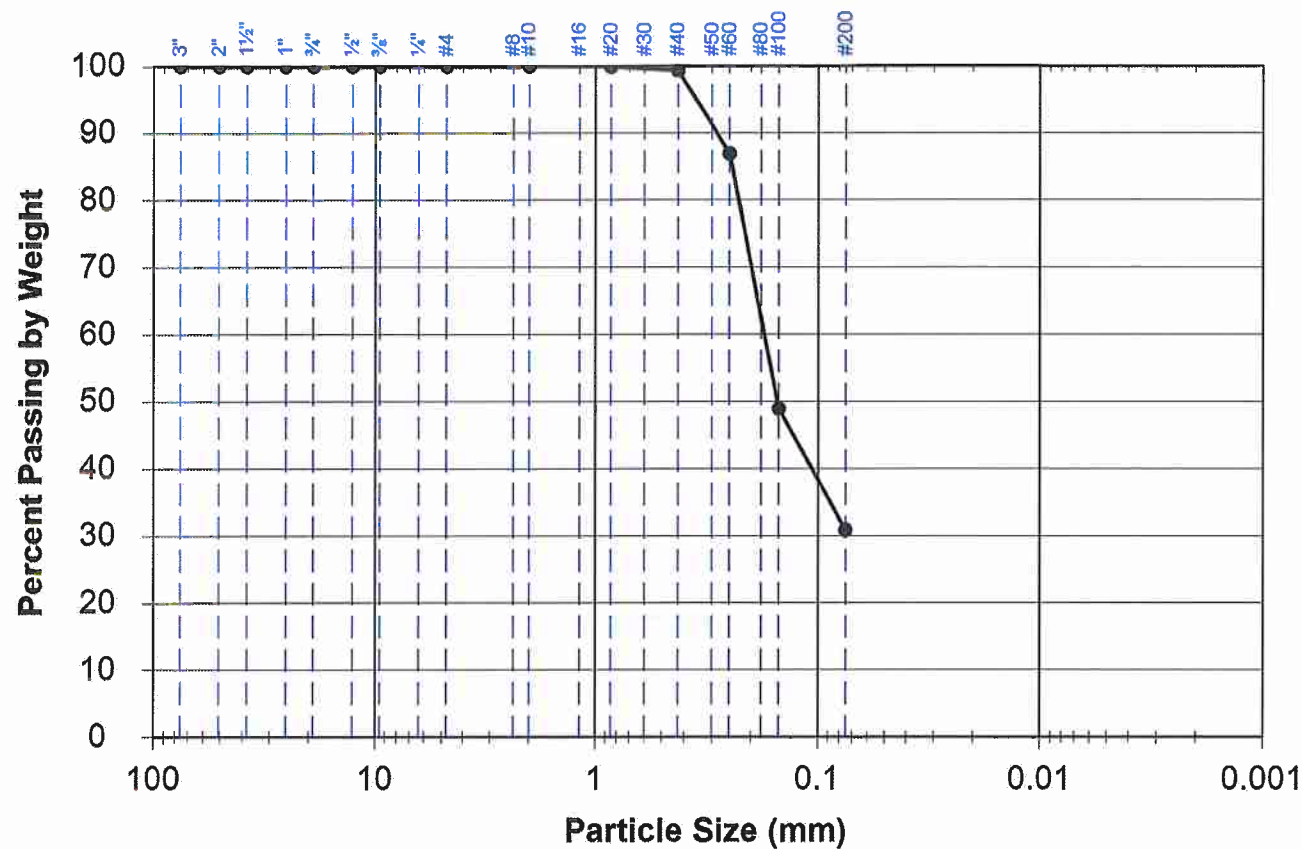
**Lab Number** 2015-364

**Received** 4/6/2015

**Reported** 4/21/2015

**Engineering Classification:** Silty Sand, SM

**Frost Classification:** Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	100%	
⅜"	100%	
¼"	100%	
#4	100%	
Total Weight of Sample 378.2g		
#10	100%	
#20	100%	
#40	99%	
#60	87%	
#100	49%	
#200	30.9%	
Total Weight of Fine Fraction 378.2g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-05  
 Sample 8  
 Depth 17.5'-19.5'

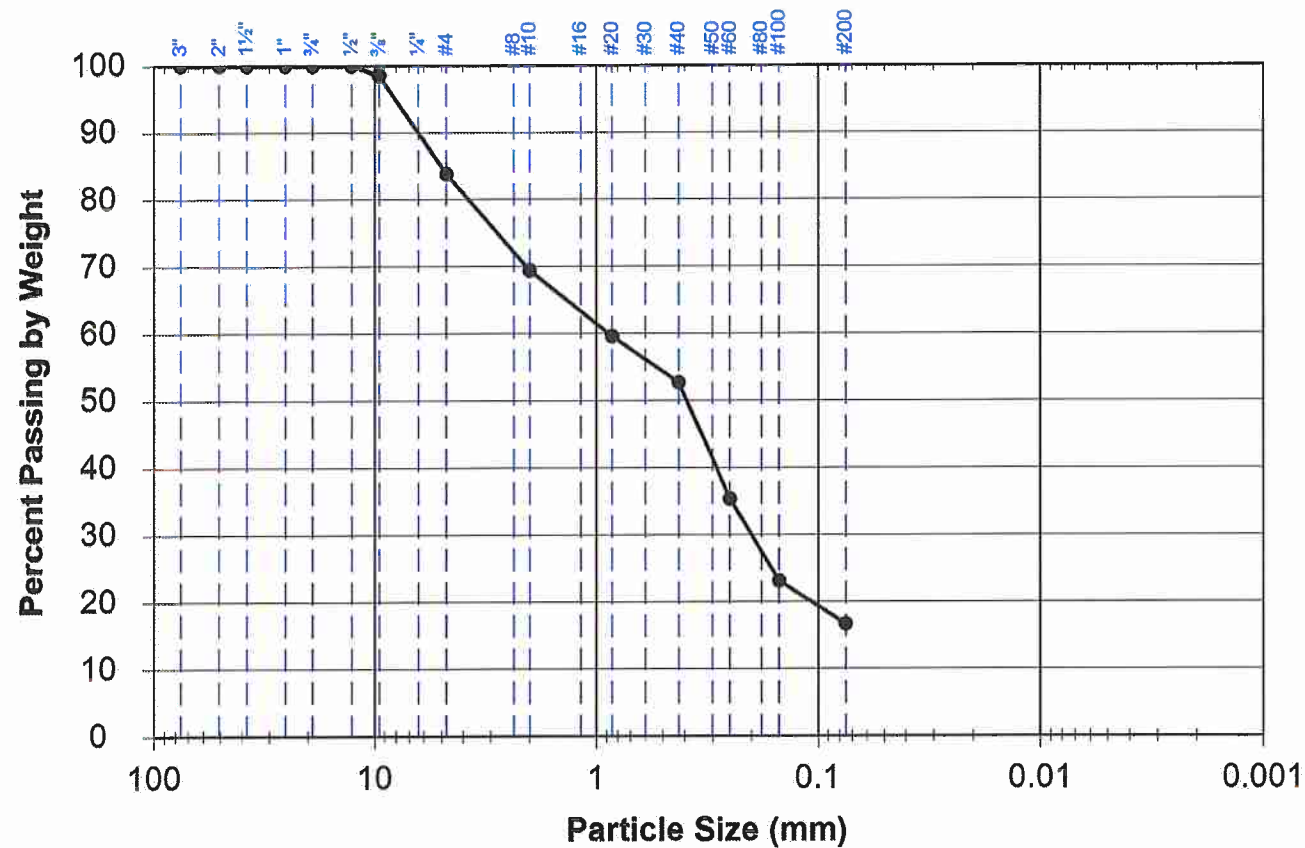
Lab Number 2015-367

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand with Gravel, SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	100%	
3/8"	99%	
#4	84%	
Total Weight of Sample 394g		
#10	69%	
#20	60%	
#40	53%	
#60	35%	
#100	23%	
#200	16.7%	
Total Weight of Fine Fraction 329.7g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-05  
 Sample 10  
 Depth 27.5'-28.1'

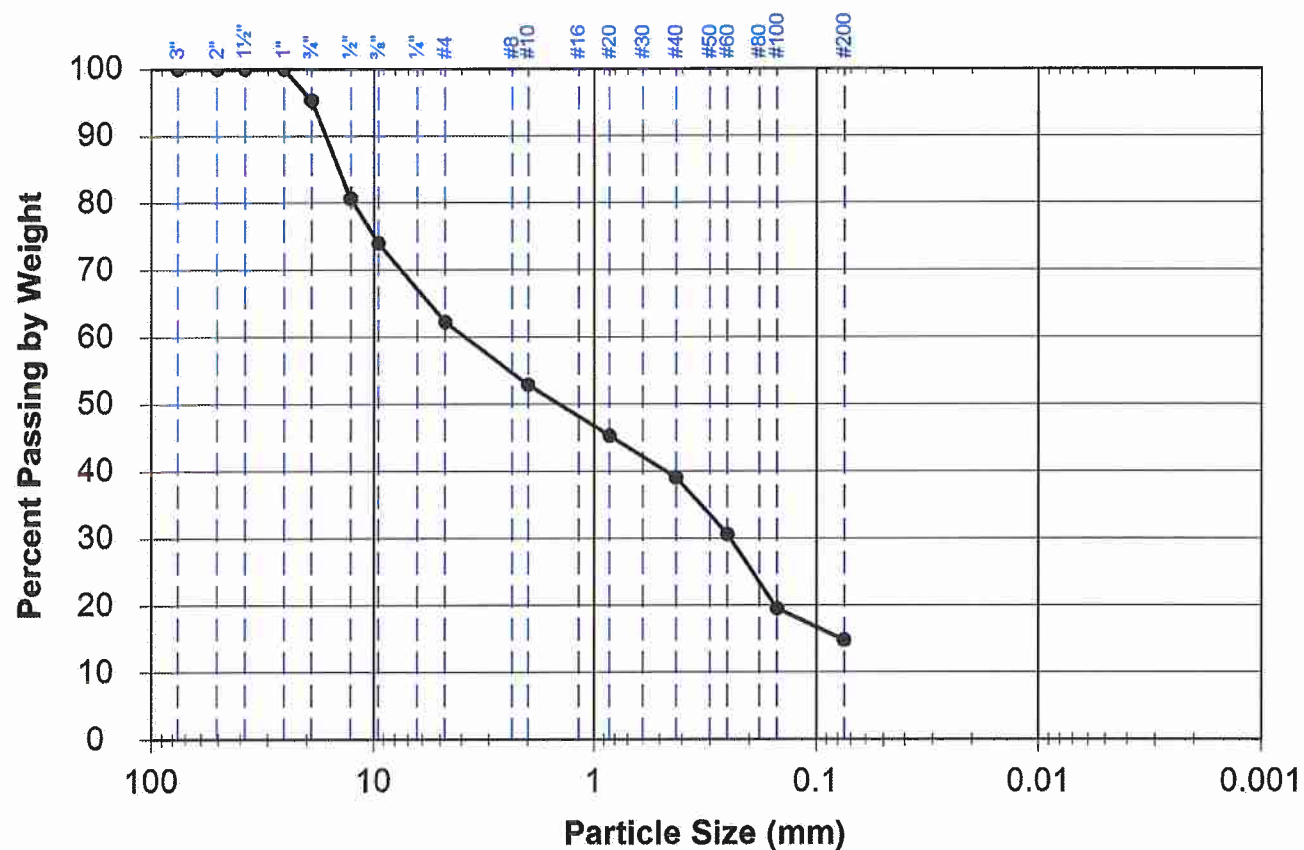
Lab Number 2015-369

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand with Gravel, SM

Frost Classification: Not Measured



Size Passing Specification

3" 100%

2" 100%

1 1/2" 100%

1" 100%

3/4" 95%

1/2" 81%

3/8" 74%

#4 62%

Total Weight of Sample 280.2g

#10 53%

#20 45%

#40 39%

#60 31%

#100 20%

#200 14.8%

Total Weight of Fine Fraction 174.3g





**Client:** Golder Associates Inc.  
**Project:** USACE Kivalina Causeway  
**Work Order:** A34316

## Particle Size Distribution

ASTM D422

**Location:** Test Borehole K15-05  
 Sample 11  
 Depth 30'-30.5'

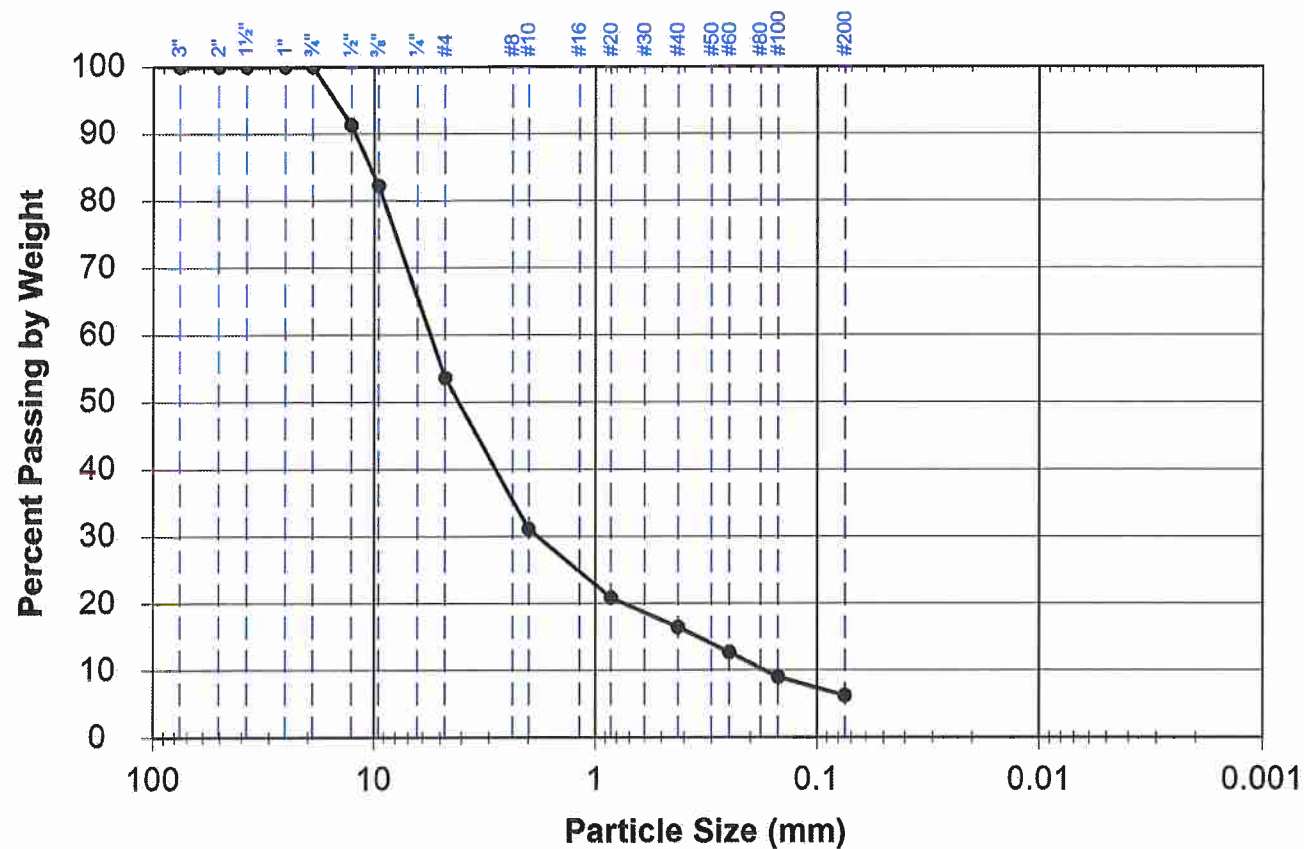
**Lab Number** 2015-370

**Received** 4/6/2015

**Reported** 4/21/2015

**Engineering Classification:** Poorly Graded Sand with Silt and Gravel, SP-SM

**Frost Classification:** Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	100%	
1/2"	91%	
3/8"	82%	
#4	54%	
Total Weight of Sample 253.1g		
#10	31%	
#20	21%	
#40	16%	
#60	13%	
#100	9%	
#200	6.3%	
Total Weight of Fine Fraction 135.6g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-06  
 Sample 3  
 Depth 5'-7'

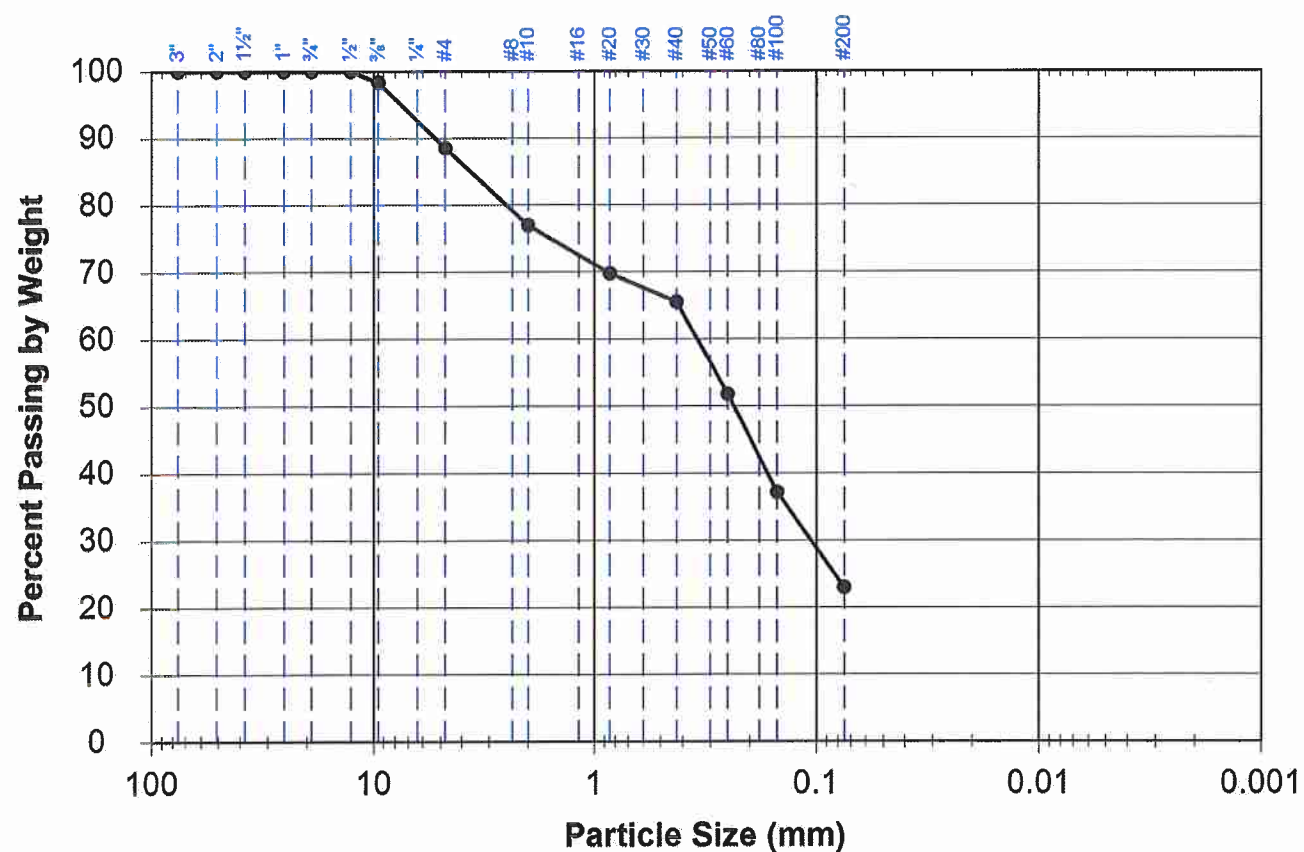
Lab Number 2015-373

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	100%	
⅜"	98%	
#4	88%	
Total Weight of Sample 404.3g		
#10	77%	
#20	70%	
#40	66%	
#60	52%	
#100	37%	
#200	23.0%	
Total Weight of Fine Fraction 357.8g		



Client: Golder Associates Inc.  
 Project: USACE Kivalina Causeway  
 Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-06  
 Sample 8  
 Depth 17.5'-19.5'

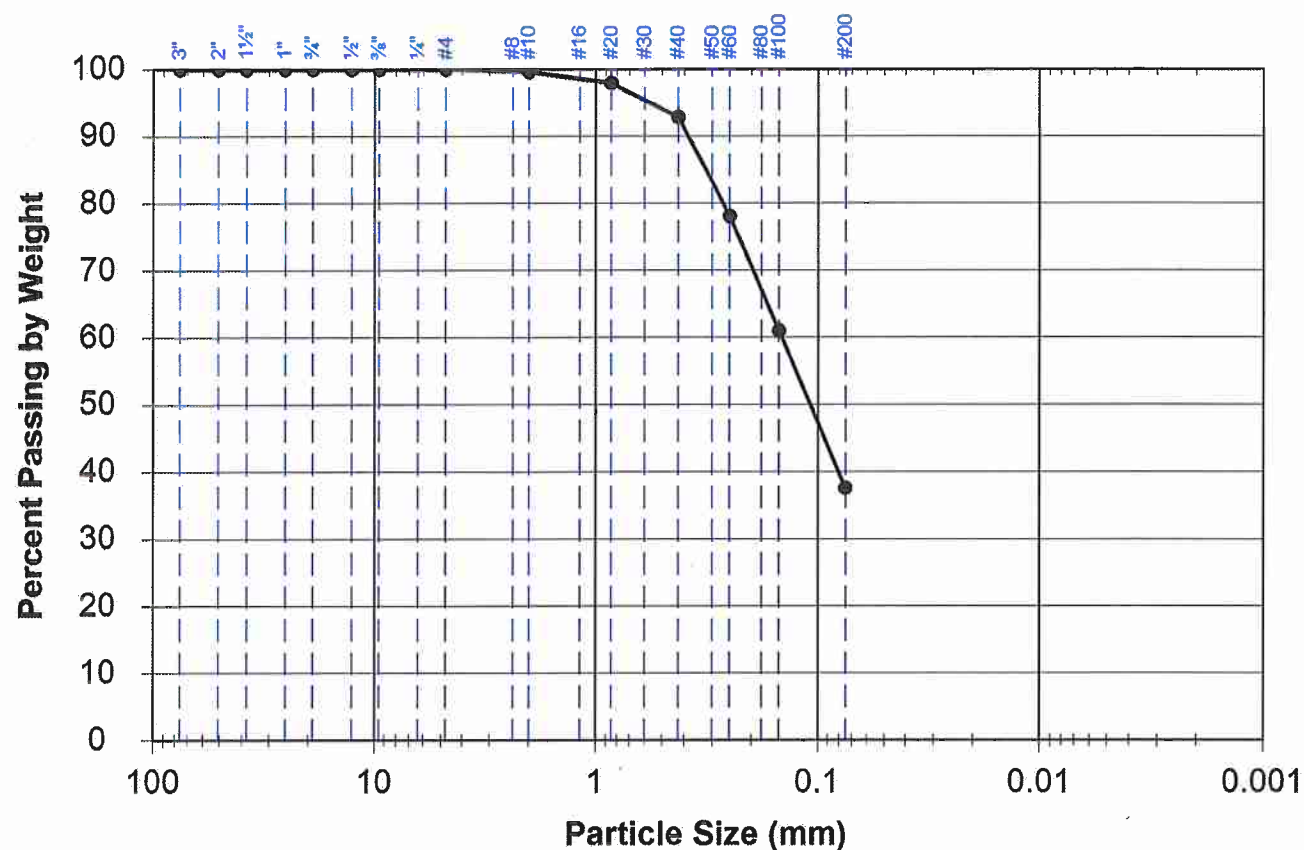
Lab Number 2015-378

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
2"	100%	
1½"	100%	
1"	100%	
¾"	100%	
½"	100%	
⅜"	100%	
¼"	100%	
#4	100%	

Total Weight of Sample 473.6g

#10	100%
#20	98%
#40	93%
#60	78%
#100	61%
#200	37.6%

Total Weight of Fine Fraction 473.6g



Client: Golder Associates Inc.  
Project: USACE Kivalina Causeway  
Work Order: A34316

## Particle Size Distribution

ASTM D422

Location: Test Borehole K15-06  
Sample 10  
Depth 27.5'-28.3'

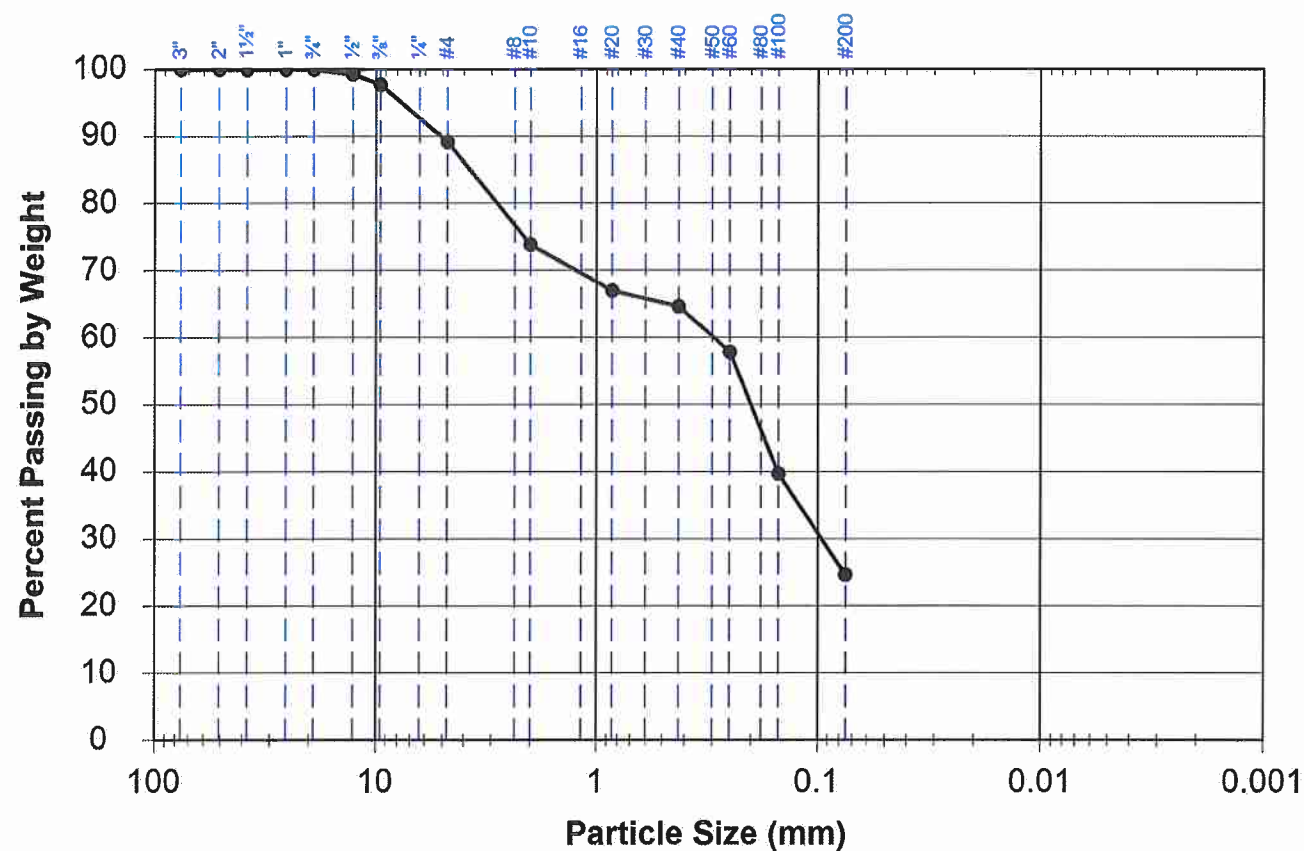
Lab Number 2015-380

Received 4/6/2015

Reported 4/21/2015

Engineering Classification: Silty Sand, SM

Frost Classification: Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
----	------	--

2"	100%	
----	------	--

1 1/2"	100%	
--------	------	--

1"	100%	
----	------	--

3/4"	100%	
------	------	--

1/2"	99%	
------	-----	--

3/8"	98%	
------	-----	--

#4	89%	
----	-----	--

Total Weight of Sample 380.8g		
-------------------------------	--	--

#10	74%	
-----	-----	--

#20	67%	
-----	-----	--

#40	65%	
-----	-----	--

#60	58%	
-----	-----	--

#100	40%	
------	-----	--

#200	24.7%	
------	-------	--

Total Weight of Fine Fraction 338.9g		
--------------------------------------	--	--



**Client:** Golder Associates Inc.  
**Project:** USACE Kivalina Causeway  
**Work Order:** A34316

## Particle Size Distribution

ASTM D422

**Location:** Test Borehole K15-06  
 Sample 11  
 Depth 30'-31'

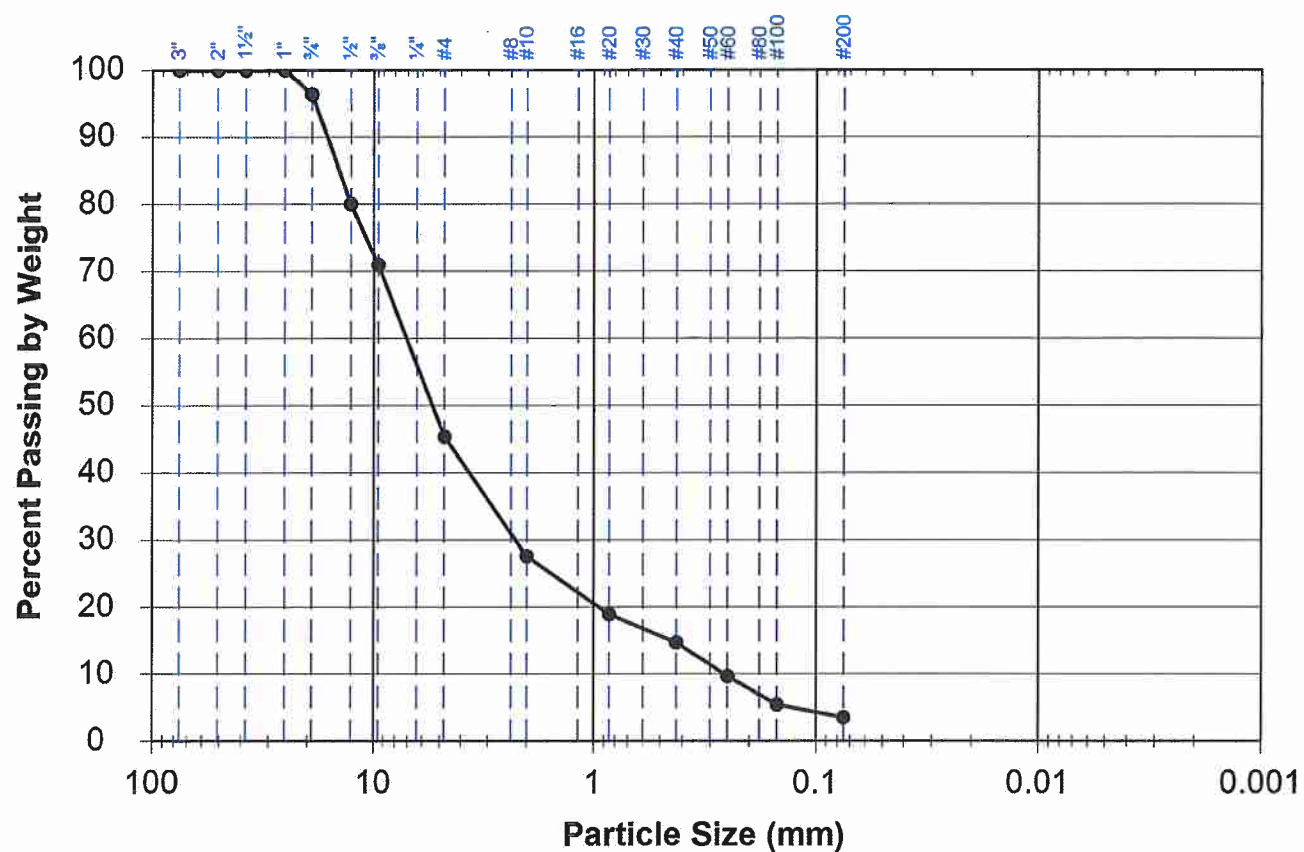
**Lab Number** 2015-381

**Received** 4/6/2015

**Reported** 4/21/2015

**Engineering Classification:** Well Graded Gravel with Sand, GW

**Frost Classification:** Not Measured



Size	Passing	Specification
------	---------	---------------

3"	100%	
2"	100%	
1 1/2"	100%	
1"	100%	
3/4"	96%	
1/2"	80%	
3/8"	71%	
#4	45%	

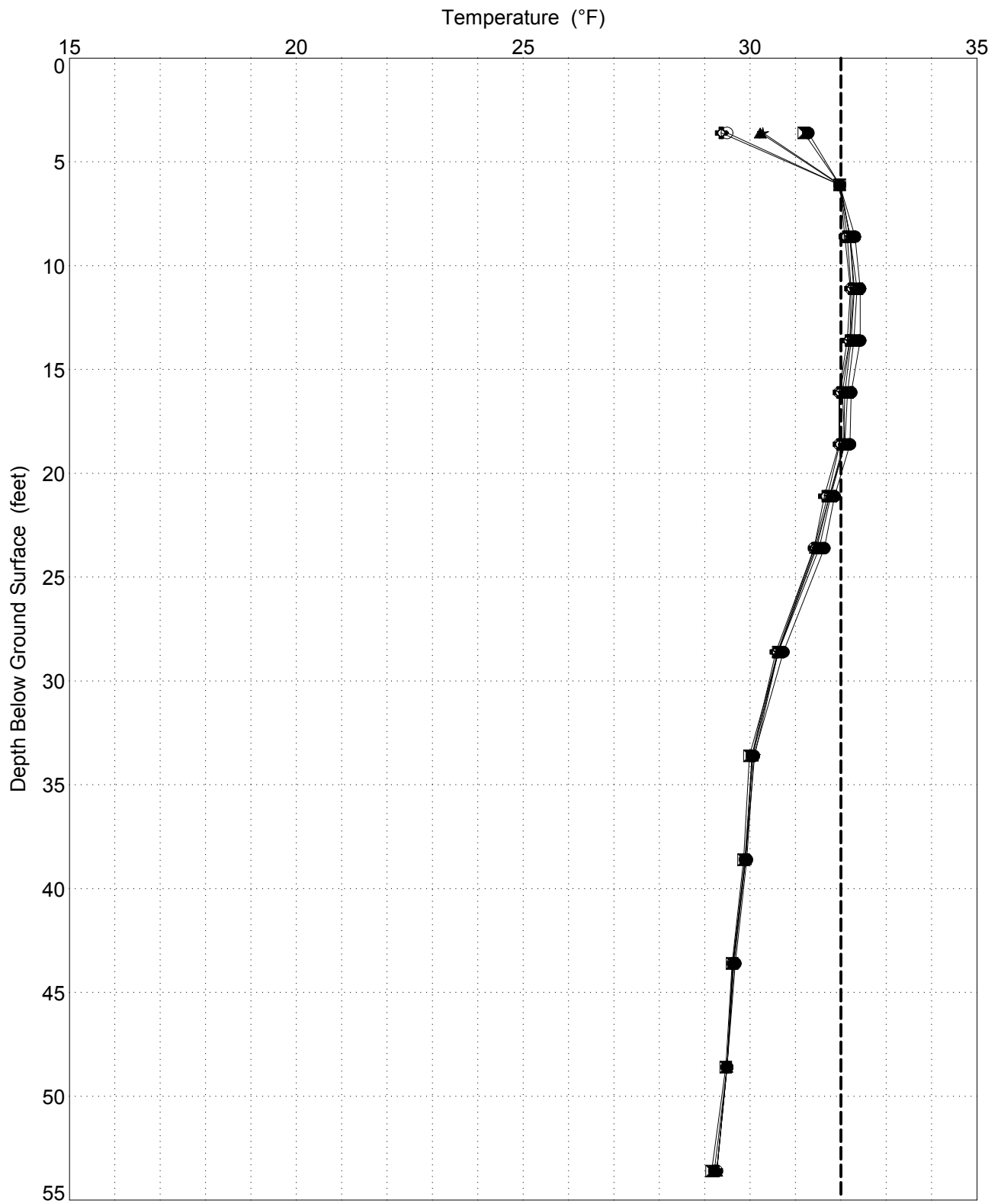
Total Weight of Sample 375.8g

#10	28%	
#20	19%	
#40	15%	
#60	10%	
#100	5%	
#200	3.5%	

Total Weight of Fine Fraction 170.5g

**APPENDIX C**  
**GROUND TEMPERATURE DATA**





● K15-01 (AP-39) 03/23/15  
 ▲ K15-01 (AP-39) 04/11/15  
 ○ K15-01 (AP-39) 04/26/15

◻ K15-01 (AP-39) 03/30/15  
 ★ K15-01 (AP-39) 04/14/15  
 ◊ K15-01 (AP-39) 05/02/15

CLIENT  
USACE

PROJECT  
KIVALINA CAUSEWAY

CONSULTANT

YYYY-MM-DD 2015-08-06

PREPARED RLCampbell

DESIGN N/A

REVIEW Howard Weston

APPROVED John Thornley



KIVALINA, AK

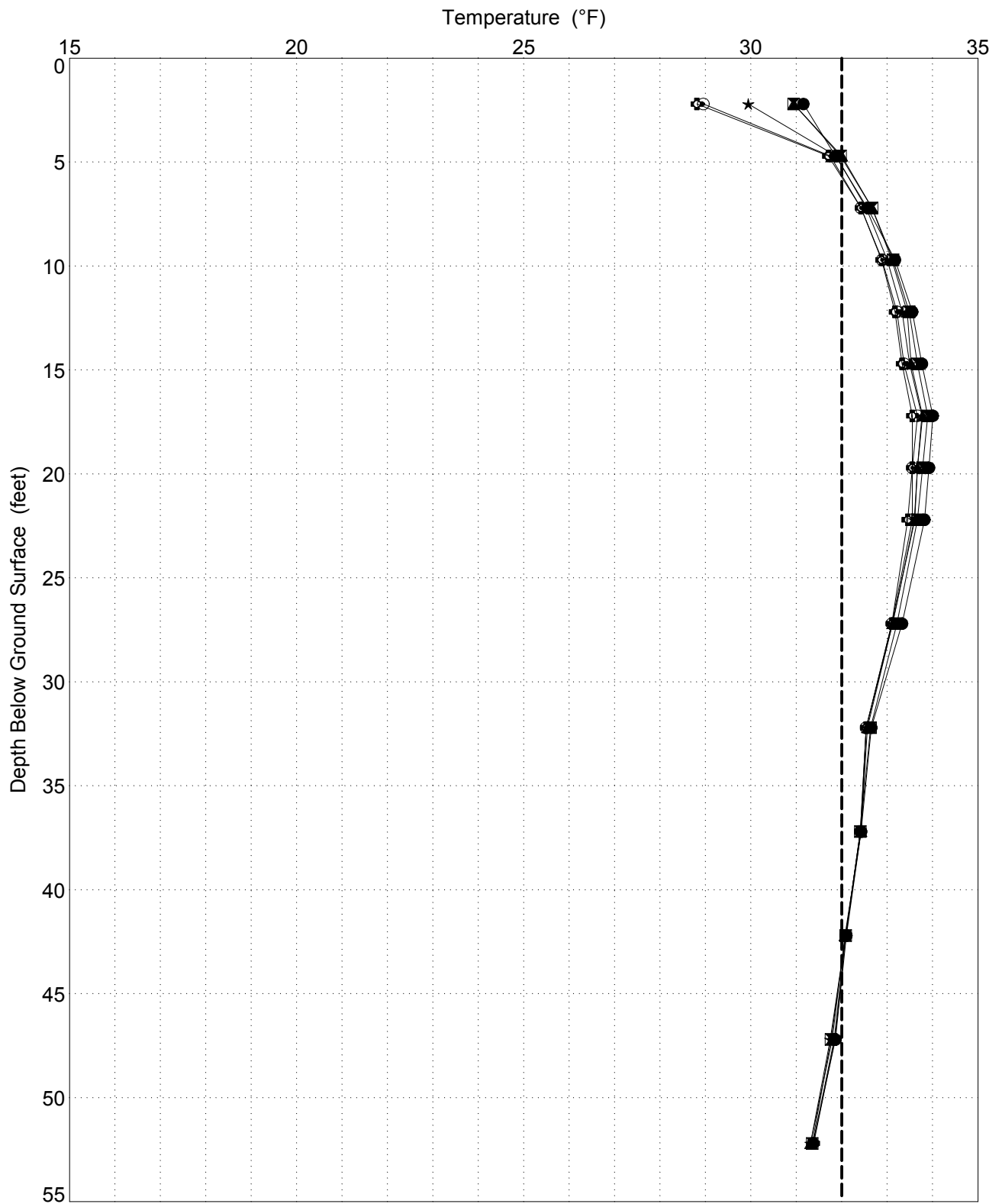
TITLE  
**MEASURED GROUND TEMPERATURES**

PROJECT No.  
1419207

CONTROL

Rev.  
----

FIGURE  
**C-1**



● K15-02 (AP-40) 03/23/15  
 ▲ K15-02 (AP-40) 04/11/15  
 ⊙ K15-02 (AP-40) 04/26/15

⊠ K15-02 (AP-40) 03/30/15  
 ★ K15-02 (AP-40) 04/14/15  
 ⊞ K15-02 (AP-40) 05/02/15

CLIENT  
USACE

PROJECT  
KIVALINA CAUSEWAY

CONSULTANT



YYYY-MM-DD 2015-08-06

PREPARED RLCampbell

DESIGN N/A

REVIEW Howard Weston

APPROVED John Thornley

KIVALINA, AK

TITLE  
**MEASURED GROUND TEMPERATURES**

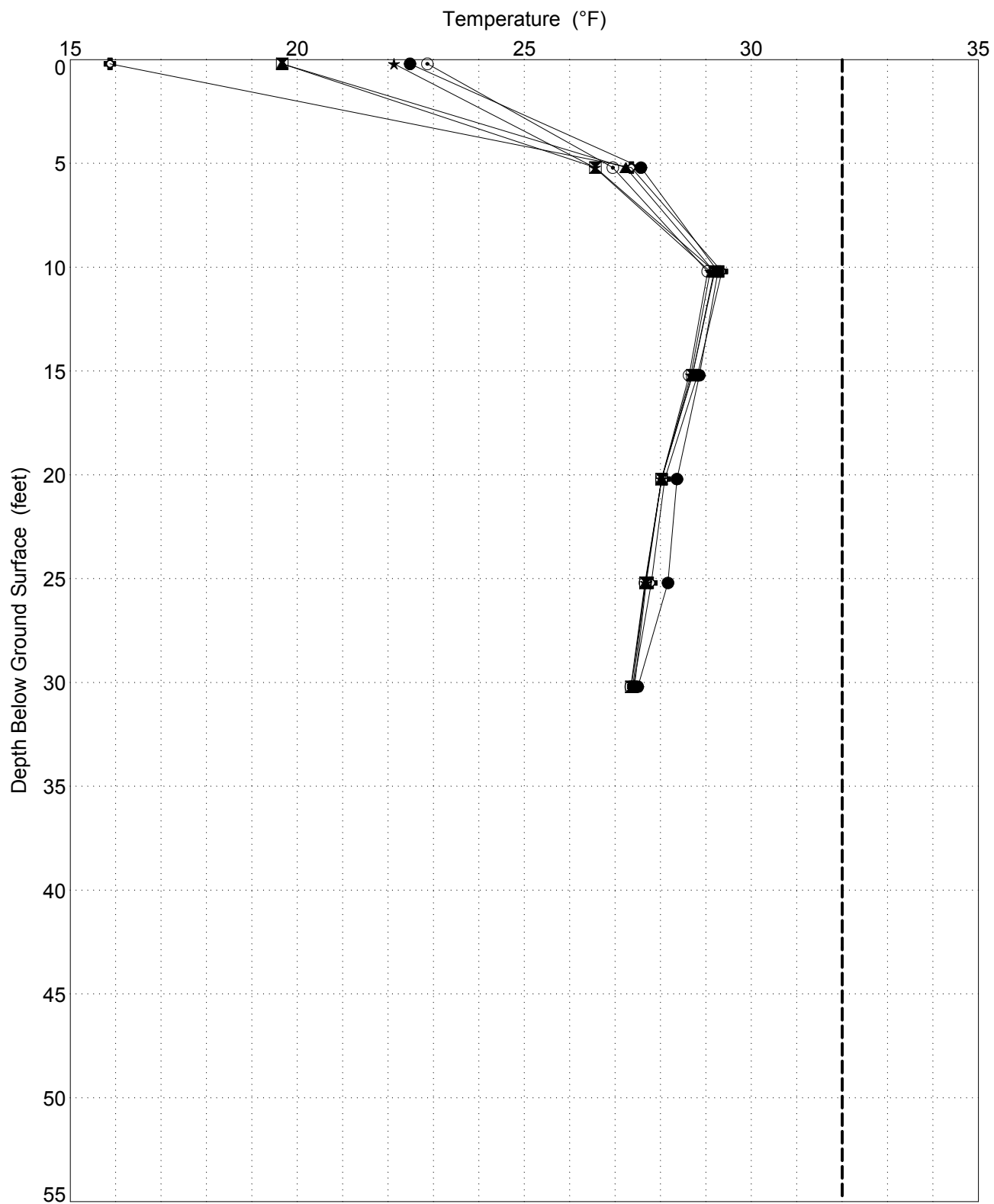
PROJECT No.  
1419207

CONTROL

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----

FIGURE  
**C-2**





● K15-06 (AP-44) 03/23/15  
 ▲ K15-06 (AP-44) 04/14/15  
 ★ K15-06 (AP-44) 04/26/15  
 ⊙ K15-06 (AP-44) 05/03/15

☒ K15-06 (AP-44) 04/12/15  
 ★ K15-06 (AP-44) 04/26/15  
 ☒ K15-06 (AP-44) 03/30/15

CLIENT  
USACE

PROJECT  
KIVALINA CAUSEWAY

CONSULTANT



YYYY-MM-DD 2015-08-06

PREPARED RLCampbell

DESIGN N/A

REVIEW Howard Weston

APPROVED John Thornley

KIVALINA, AK

TITLE  
**MEASURED GROUND TEMPERATURES**

PROJECT No.  
1419207

CONTROL

Rev.  
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FIGURE  
**C-3**

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